

Steady radial ice-sheet flow with fabric evolution

Leslie W. MORLAND,¹ Ryszard STAROSZCZYK²

¹*School of Mathematics, University of East Anglia, Norwich NR4 7TJ, UK*

²*Institute of Hydro-Engineering, Polish Academy of Sciences, ul. Waryńskiego 17, 71-310 Szczecin, Poland
E-mail: rstar@ibwpan.gda.pl*

ABSTRACT. Reorientation of individual crystal glide planes, as isotropic surface ice is deformed during its passage to depth in an ice sheet, creates a fabric and associated anisotropy. We adopt an evolving orthotropic viscous law which was developed to reflect the induced anisotropy arising from the mean rotation of crystal axes during deformation. This expresses the deviatoric stress in terms of the strain rate, strain and three structure tensors based on the principal stretch axes, and involves one fabric response function which determines the strength of the anisotropy. The initial isotropic response enters as a multiplying factor depending on a strain-rate invariant and incorporating a temperature-dependent rate factor. The fabric response function has been constructed by correlations with complete (idealized) uniaxial compression and shearing responses for both 'cold' and 'warm' ice. The possible effects of such fabric evolution are now illustrated by determining steady radially symmetric flow solutions for an ice sheet with a prescribed temperature distribution and subject to an elevation-dependent surface accumulation/ablation distribution, zero basal melting and a prescribed basal sliding law. Comparisons are made with solutions for the conventional isotropic viscous law, for a flat bed, for a bed with a single modest slope hump and for a bed with a single modest slope hollow, for both cold and warm ice.

1. INTRODUCTION

Ice-core samples taken from depth in an ice sheet reveal strong fabrics, shown by significant alignment of initially randomly distributed c axes of individual crystals, and consequently substantial differences in shear viscosities in different planes. A macroscopic viscous law for the shear stress proposed by Morland and Staroszczyk (1998) was motivated by a simple picture of the rotational recrystallization in which individual crystal glide planes, material planes, are rotated towards planes normal to principal axes of compression, and away from planes normal to principal axes of extension, described as the principal stretch planes. The instantaneous viscous response at each stage of the deformation has reflexional symmetry in these planes; that is, the instantaneous viscous response is orthotropic with respect to the current principal stretch planes. The directional strengths of the response depend on the current deformation. The orthotropic viscous law is then a frame-indifferent relation between deviatoric stress, strain rate, deformation and the three structure tensors defined by the outer products of the three orthogonal unit vectors along the principal stretch axes. Subsequently, a set of equalities and inequalities on the instantaneous directional viscosities was derived from the rotation concepts by Staroszczyk and Morland (2000), designated by one author (L.W.M.) as the 'Staroszczyk inequalities', which showed that at least two tensor generators in the orthotropic law were required. Further refinements (Staroszczyk and Morland, 2001; Morland and Staroszczyk, 2003) led to a model law with two tensor generators, each with a fabric response coefficient function, but with an equality from the Staroszczyk inequalities providing an explicit relation between the two functions, so only one fabric response function need be prescribed. Two such model functions were constructed by

correlation with complete (idealized) monotonic uniaxial compression and shearing responses which satisfy observed limit viscosity enhancement factors associated with cold and warm ice. The initial isotropic response enters as a multiplying factor depending on a strain-rate invariant and incorporating a temperature-dependent rate factor.

While this fabric-evolution model ignores such effects as grain growth and temperature variation during the evolution, it is adopted here to illustrate, for the first time, the possible significance of fabric effects included in the determination of an ice-sheet flow, with the cold- and warm-ice models reflecting contrasting influences. We have investigated steady radially symmetric flow to restrict the system of partial differential equations to two independent variables, horizontal and vertical spatial coordinates, which allow accurate numerical solution. This incorporates a realistic lateral spreading which is lost in the simpler plane flow equations. The adopted temperature field is prescribed in terms of surface elevation and depth below surface, such that there is uniform heat flux into the base and a constant rate of temperature decrease with elevation at the surface. The applied elevation-dependent surface accumulation/ablation increases exponentially with elevation from large ablation at the margin to smaller accumulation at the divide. The prescribed basal sliding law is a linear relation between the basal tangential traction and velocity, with coefficient proportional to the normal traction which eliminates a surface slope singularity at the margin. The theory allows a prescribed basal melting/refreezing distribution, but this is assumed zero in the illustrations.

We also consider bed topography of modest slope relative to the horizontal mean bed plane. Morland (2000) derived the enhanced reduced model for steady plane isothermal linearly viscous flow over beds of moderate slope, δ , which are the leading order balances in asymptotic expansions of

the full system of equations and boundary conditions, depending on the very small surface slope, ϵ , and on the allowed larger topography slope, δ ($\epsilon \ll \delta \ll 1$), and on s , the topography span relative to the sheet thickness, where $1 \lesssim s \lesssim 1/\delta$. The error magnitude is of order δ/s . The expansions were generalized for prescribed temperature and non-linear viscous flow by Morland (2001), obtaining the same error magnitude. We now derive the analogous leading order balances, an enhanced reduced model, with the above anisotropic viscous law incorporating fabric evolution. The error magnitude is now of order δ , which is greater than before when $s \gg 1$; hence the description 'modest slope'. Illustrations, and comparisons with the isotropic theory, are presented for both the cold- and warm-ice models, for a flat bed, a bed with a single hump of maximum slope $\delta = 0.01$ and a bed with a single hollow of maximum slope $\delta = 0.01$.

The numerical procedure is a non-trivial iteration between the hyperbolic partial differential equations governing the fabric evolution for a given velocity field, starting with the isotropic flow solution, and the solution of the two-point boundary-value problem given by the enhanced reduced model for the flow with given fabric. The final solution criterion is that the relative changes of margin radius, divide height and mean thickness are all less than 10^{-5} . Full details of the numerical methods are presented in section 7.

2. FABRIC EVOLUTION ANISOTROPIC VISCOUS LAW

2.1. Initial isotropic response

The initial isotropic response is defined by a non-linear viscous, incompressible, fluid relation between the strain-rate tensor \mathbf{D} and the deviatoric stress tensor $\hat{\boldsymbol{\sigma}}$, with a temperature-dependent rate factor $a(T)$, where T is absolute temperature. The deviatoric stress is defined in terms of the Cauchy stress, $\boldsymbol{\sigma}$, and mean pressure, p , by

$$\hat{\boldsymbol{\sigma}} = \boldsymbol{\sigma} + p\mathbf{I}, \quad 3p = -\text{tr}\boldsymbol{\sigma}, \quad \text{tr}\hat{\boldsymbol{\sigma}} = 0, \quad (1)$$

where \mathbf{I} is the unit tensor. The conventional simplifications that \mathbf{D} is parallel to $\hat{\boldsymbol{\sigma}}$, and the viscosity coefficient depends only on the second principal invariant of $\hat{\boldsymbol{\sigma}}$, or of \mathbf{D} , are adopted. The equivalent stress and strain-rate formulations of the viscous law are

$$\frac{\hat{\boldsymbol{\sigma}}}{\sigma_0} = \phi(\tilde{I}) \frac{\bar{\mathbf{D}}}{D_0}, \quad \frac{\bar{\mathbf{D}}}{D_0} = \psi(J) \frac{\hat{\boldsymbol{\sigma}}}{\sigma_0}, \quad (2)$$

$$\tilde{I} = \frac{1}{2} \text{tr} \left(\frac{\bar{\mathbf{D}}}{D_0} \right)^2, \quad J = \frac{1}{2} \text{tr} \left(\frac{\hat{\boldsymbol{\sigma}}}{\sigma_0} \right)^2,$$

where $\bar{\mathbf{D}}$ is an effective strain rate defined by

$$\bar{\mathbf{D}} = a(T) \mathbf{D}. \quad (3)$$

The units σ_0 and D_0 are chosen, with unit rate factor a at the melting temperature, so that the constitutive functions $\psi(J)$ and $\phi(\tilde{I})$ are of order unity for deviatoric stresses and strain rates arising in typical ice-sheet flows,

$$\sigma_0 = 10^5 \text{ N m}^{-2}, \quad D_0 = 1 \text{ a}^{-1} = 3.17 \times 10^{-8} \text{ s}^{-1}. \quad (4)$$

Given a monotonic $\phi(\tilde{I})$ or $\psi(J)$, there is a unique monotonic $\psi(J)$ or $\phi(\tilde{I})$, respectively, satisfying, from (2), the relations

$$\phi(\tilde{I})\psi(J) = 1, \quad \tilde{I} = J\psi^2(J), \quad J = \tilde{I}\phi^2(\tilde{I}). \quad (5)$$

The pressure, p , is a workless constraint not given by a

constitutive law, but determined by momentum balance and boundary conditions.

An accurate approximation to the Glen (1955) data over a shear stress range $0-5 \times 10^5 \text{ N m}^{-2}$, $0 \leq J \leq 25$, is given by the polynomial representation for $\psi(J)$ determined by Smith and Morland (1981):

$$\psi(J) = 0.3336 + 0.32J + 0.02963J^2. \quad (6)$$

This has the mathematical advantage of a finite viscosity at zero stress, unlike the power law proposed by Glen (1955), and is adopted here. We will show that the enhanced reduced model in fact requires only the function $\psi(J)$, and not $\phi(\tilde{I})$, for the isotropic response, even though the asymptotic analysis with the anisotropic law starts from the expression for stress. They also derived an accurate representation for $a(T)$ from data presented by Mellor and Testa (1969) for temperatures between melting and 60 K below melting. A good simplifying approximation of that representation over the range of practical significance from melting to 40 K below melting is

$$a(T) = 0.68 \exp(12\bar{T}) + 0.32 \exp(3\bar{T}), \quad (7)$$

$$T = 273.15 \text{ K} + [20 \text{ K}] \bar{T},$$

which is adopted here. The dimensionless temperature \bar{T} is zero at melting, and -2 at 40 K below melting.

2.2. Orthotropic viscous law

For direct application to the momentum balances of ice-sheet flows, a constitutive law for the stress is required. The law adopted here is that proposed by Morland and Staroszczyk (2003), in which the fabric is governed by the evolution of the left Cauchy–Green strain tensor $\mathbf{B} = \mathbf{F}\mathbf{F}^T$, where \mathbf{F} is the deformation gradient and the superscript 'T' denotes transpose of a tensor. Let Ox_i ($i = 1, 2, 3$) be spatial rectangular Cartesian coordinates with Ox_i ($i = 1, 2, 3$) particle reference coordinates, and v_i the velocity components, then the deformation gradient \mathbf{F} , spatial velocity gradient \mathbf{L} and strain rate \mathbf{D} have components

$$F_{ij} = \frac{\partial x_i}{\partial X_j}, \quad L_{ij} = \frac{\partial v_i}{\partial x_j}, \quad D_{ij} = \frac{1}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right). \quad (8)$$

The kinematic relation for \mathbf{B} is

$$\frac{D\mathbf{B}}{Dt} = \mathbf{L}\mathbf{B} + \mathbf{B}\mathbf{L}^T, \quad (9)$$

where t denotes time and the notation D/Dt denotes a material time derivative. In practice, (9) must be solved simultaneously with the momentum balance and constitutive law, and is subject to an initial condition that $\mathbf{B} = \mathbf{F} = \mathbf{I}$, the unit tensor, when the ice is first deposited at the surface. The orthogonal unit vectors $\mathbf{e}^{(l)}$ ($l = 1, 2, 3$) defining the principal stretch axes, and the squares b_l ($l = 1, 2, 3$) of the principal stretches, are defined by

$$\mathbf{B}\mathbf{e}^{(l)} = b_l\mathbf{e}^{(l)}, \quad \det(\mathbf{B} - b_l\mathbf{I}) = 0. \quad (10)$$

The latter relation is a cubic equation with positive roots. By incompressibility,

$$\text{div} \mathbf{v} = 0, \quad \det \mathbf{B} = b_1 b_2 b_3 = 1. \quad (11)$$

An orthotropic, with respect to the principal stretch planes, viscous law for the deviatoric stress $\hat{\boldsymbol{\sigma}}$ is a frame-indifferent relation depending on the strain-rate tensor \mathbf{D} , the left

Cauchy–Green strain tensor \mathbf{B} , and three structure tensors $\mathbf{M}^{(l)}$ defined by the outer products of the current principal stretch axes unit vectors $\mathbf{e}^{(l)}$ ($l = 1, 2, 3$),

$$\mathbf{M}^{(l)} = \mathbf{e}^{(l)} \otimes \mathbf{e}^{(l)}, \quad (l = 1, 2, 3). \quad (12)$$

A key feature of the law proposed by Morland and Staroszczyk (2003) is the choice of the invariant arguments for the two fabric response coefficient functions, for which the directional viscosity equality yields an explicit algebraic relation between the two functions. These invariants are

$$\xi_l = b_l - 1/b_l \quad (l = 1, 2, 3), \quad \eta = \sqrt{(K - 1)^2 - 4}, \quad (13)$$

where

$$K = \text{tr} \mathbf{B} = b_1 + b_2 + b_3,$$

instead of the previous invariants b_l and K used in earlier formulations by Staroszczyk and Morland (2000, 2001). Henceforth omitting the subscript ' l ' for common relations, the invariants have the properties

$$\xi \rightarrow -\infty \text{ as } b \rightarrow 0, \quad \xi = 0 \text{ at } b = 1, \quad \xi \rightarrow \infty \text{ as } b \rightarrow \infty, \\ \eta \geq 0, \quad \eta = 0 \text{ at } K = 3, \quad \eta \sim K \rightarrow \infty \text{ as } K \rightarrow \infty.$$

The proposed stress formulation is then

$$\hat{\sigma} = 2\mu \left\{ \bar{\mathbf{D}} + \sum_{l=1}^3 \bar{f}(\xi_l) [\mathbf{M}^{(l)} \bar{\mathbf{D}} + \bar{\mathbf{D}} \mathbf{M}^{(l)} - \frac{2}{3} \text{tr}(\mathbf{M}^{(l)} \bar{\mathbf{D}}) \mathbf{I}] \right. \\ \left. + \bar{g}(\eta) [\bar{\mathbf{D}} \mathbf{B} + \mathbf{B} \bar{\mathbf{D}} - \frac{2}{3} \text{tr}(\bar{\mathbf{D}} \mathbf{B}) \mathbf{I}] \right\}, \quad (14)$$

where μ is the isotropic viscosity function defined by

$$\mu = \frac{\sigma_0}{2D_0} \phi(\tilde{I}) = \frac{\sigma_0}{2D_0} \psi^{-1}(J), \quad (15)$$

and $\bar{f}(\xi_l)$ and $\bar{g}(\eta)$ are the fabric response coefficients. The dependence of the coefficient \bar{f} for the term involving $\mathbf{M}^{(l)}$ on b_l alone, and the dependence of the coefficient \bar{g} on an isotropic invariant, chosen to be K , were deduced (Morland and Staroszczyk, 1998) from symmetry conditions on the directional viscosities as the b_l are permuted. Note that the law (14) makes the simplifying assumptions that the temperature influences both the rate of strain and the fabric evolution only through the effective strain rate, i.e. with a common rate factor $a(T)$, and that the anisotropic part also has the isotropic viscosity function μ as a multiplying factor. The vanishing of the anisotropic part when $\mathbf{B} = \mathbf{I}$ gives the normalization condition

$$\bar{f}(0) + \bar{g}(0) = 0. \quad (16)$$

Bounded response as $b_l \rightarrow \infty$, hence K and $\eta \rightarrow \infty$, implies $\bar{g}(\eta) \sim \eta^{-1}$ as $\eta \rightarrow \infty$, and it is convenient to introduce the alternative fabric response function $\bar{G}(\eta)$ defined by

$$\bar{G}(\eta) = \eta \bar{g}(\eta), \quad (17)$$

where $\bar{G}(\eta)$ is finite and non-zero as $\eta \rightarrow \infty$. The non-trivial directional viscosity equality (Morland and Staroszczyk, 2003) with this choice of invariant arguments gives an explicit relation for $\bar{G}(\eta)$ in terms of $\bar{f}(\eta)$; namely,

$$\bar{G}(\eta) = \eta \bar{g}(\eta) = -\bar{f}(\eta) + \bar{f}(-\eta) = -2\bar{f}^o(\eta), \quad \eta \geq 0, \quad (18)$$

where \bar{f}^o is the odd part of $\bar{f}(\xi)$ (\bar{f}^e is the even part). That is, in terms of the new invariant arguments, $\bar{g}(\eta)$ is determined explicitly in terms of $\bar{f}^o(\eta)$, and the constitutive law can be expressed directly in terms of a single independent fabric

response function $\bar{f}(\xi)$. The limit of (18) as $b_l \rightarrow 1$, $\eta \rightarrow 0$, together with the normalization (16), shows that

$$\bar{G}(0) = 0, \\ \bar{g}(0) = -\bar{f}(0) = -\bar{f}^e(0) = -2\bar{f}'(0) = -2\bar{f}'^o(0), \quad (19)$$

which is a restriction on $\bar{f}(\xi)$ at $\xi = 0$; the prime denotes an ordinary derivative of a function with respect to its argument.

2.3. Uniaxial compression and shear limits

Budd and Jacka (1989) and Li and others (1996) have experimentally determined the limit ratios of fabric-induced viscosity to isotropic viscosity for indefinite axial compression with equal unconfined lateral extensions, and for indefinite shear in a plane deformation, A and S , respectively. Since these experiments were near melting temperature, we use the term warm ice. In contrast, Mangeney and others (1996) deduced values of A and S from the ice-core data of Thorsteinsson and others (1997), for which we use the term cold ice. The reciprocals of these ratios, A^{-1} and S^{-1} , are described as enhancement factors. While the warm-ice experiments showed A to be less than unity, the cold-ice-core measurements showed A to be greater than unity. Here we adopt the parameters inferred by Morland and Staroszczyk (2003) from the above,

$$\begin{aligned} \text{cold ice:} \quad A = 3, \quad S = 1/5; \\ \text{warm ice:} \quad A = 1/3, \quad S = 1/8. \end{aligned} \quad (20)$$

The uniaxial and shear ratios given by (14) provide two more restrictions on the limit values of $\bar{f}(\xi)$ and $\bar{G}(\eta)$, which combine to give (Morland and Staroszczyk, 2003)

$$\begin{aligned} \bar{f}^e(\infty) &= (3A - 2S - 1)/2, \\ \bar{G}(\infty) &= -2\bar{f}^o(\infty) = 3(S - A), \end{aligned} \quad (21)$$

from which, with the parameters (20),

$$\text{cold ice:} \quad \bar{f}^o(\infty) = 4.2, \quad \bar{f}(\infty) = 8; \quad (22)$$

$$\text{warm ice:} \quad \bar{f}^o(\infty) = 0.3125, \quad \bar{f}(\infty) = 0.1875. \quad (23)$$

2.4. Fabric response functions

Morland and Staroszczyk (2003) assumed, since data for the full uniaxial and shear responses are not known, that both responses varied exponentially between their known initial and limit values, and determined a corresponding fabric function $\bar{f}(\xi)$, of order unity by construction, by least-squares correlation with both responses for both warm and cold ice.

For warm ice, the correlation gave

$$\bar{f}(\xi) = \bar{f}(\infty) - 2\bar{f}^o(\infty) \exp[-\alpha q(b)], \quad (24)$$

where

$$2b = \xi + \sqrt{\xi^2 + 4}, \quad q(b) = \sum_{n=1}^5 a_n b^{c_n}, \quad \alpha, a_n, c_n > 0,$$

and

$$a_1 = 0.0106, \quad a_2 = 28.856, \quad a_3 = 0.2770,$$

$$a_4 = 0.8920, \quad a_5 = 7.1065;$$

$$c_1 = 27.061, \quad c_2 = 2.4772, \quad c_3 = 2.4506,$$

$$c_4 = 27.021, \quad c_5 = 2.4727;$$

$$\alpha = 0.1003.$$

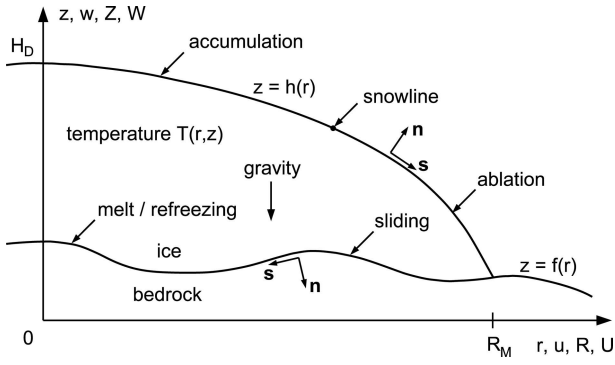


Fig. 1. Ice-sheet geometry.

For cold ice, the correlation gave

$$\bar{f}^e(\xi) = \bar{f}^e(\infty) + \bar{f}^o(\infty) \sum_{n=1}^5 \frac{a_n}{1 + c_n(\xi/b_*)^{2n}}, \quad (25)$$

where

$$\begin{aligned} a_1 &= -0.1616, & a_2 &= 0.0332, & a_3 &= 0.0587, \\ a_4 &= -0.0634, & a_5 &= -0.0727; \\ c_1 &= 5.2828, & c_2 &= 1045.581, & c_3 &= 0.0005, \\ c_4 &= 20.953, & c_5 &= 0.1952; \\ b_* &= 4. \end{aligned}$$

3. AXIALLY SYMMETRIC FLOW

Steady axisymmetric flow of a large ice sheet is described by the radial and vertical velocity fields, $u(r, z)$ and $w(r, z)$, respectively, where r is a horizontal radial coordinate and z is a vertically upward distance coordinate of cylindrical polar coordinates (r, θ, z) , and all the flow variables are independent of the polar angle, θ . The corresponding non-zero physical components of the strain rate are

$$\begin{aligned} D_{rr} &= \frac{\partial u}{\partial r}, & D_{\theta\theta} &= \frac{u}{r}, & D_{zz} &= \frac{\partial w}{\partial z}, \\ D_{rz} &= \frac{1}{2} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial r} \right), \end{aligned} \quad (26)$$

subject to the assumption of incompressibility, equivalent to the mass-balance condition,

$$D_{rr} + D_{\theta\theta} + D_{zz} = 0, \quad \frac{\partial u}{\partial r} + \frac{u}{r} + \frac{\partial w}{\partial z} = 0, \quad (27)$$

which is satisfied identically by expressing the velocity components in terms of a stream function, $\omega(r, z)$,

$$u = \frac{1}{r} \frac{\partial \omega}{\partial z}, \quad w = -\frac{1}{r} \frac{\partial \omega}{\partial r}. \quad (28)$$

The horizontal radial and vertical momentum balances for the very slow flow in which acceleration terms are negligible are, respectively,

$$\begin{aligned} -\frac{\partial p}{\partial r} + \frac{\partial \hat{\sigma}_{rr}}{\partial r} + \frac{\hat{\sigma}_{rr} - \hat{\sigma}_{\theta\theta}}{r} + \frac{\partial \hat{\sigma}_{rz}}{\partial z} &= 0, \\ -\frac{\partial p}{\partial z} + \frac{\partial \hat{\sigma}_{zz}}{\partial z} + \frac{\partial \hat{\sigma}_{rz}}{\partial r} + \frac{\hat{\sigma}_{rz}}{r} - \rho g &= 0, \end{aligned} \quad (29)$$

where $\rho = 918 \text{ kg m}^{-3}$ is the constant ice density, $g = 9.81 \text{ m s}^{-2}$ is the constant gravity acceleration, and the circumferential momentum balance is automatically satisfied.

It is supposed that the atmospheric pressure at the surface is uniform, and stress is measured relative to this pressure. Then the ice-sheet surface $z = h(r)$ is traction-free, and is subjected to a normal net ice flux q_n , which is positive over accumulation zones and negative over ablation zones. It is expected that accumulation will occur over a central zone at higher elevations, and ablation below a snowline. In general, q_n will depend on elevation h and location r . Let the surface have unit tangent and outward normal vectors \mathbf{s} and \mathbf{n} in a righthand sense, then

$$\begin{aligned} \mathbf{n} &= \Delta_h^{-1} [-h'(r), 0, 1], & \mathbf{s} &= \Delta_h^{-1} [1, 0, h'(r)], \\ \Delta_h &= \left\{ 1 + [h'(r)]^2 \right\}^{\frac{1}{2}}. \end{aligned} \quad (30)$$

The zero traction is conveniently expressed in terms of vanishing normal and tangential tractions $t_n = \mathbf{n} \times \boldsymbol{\sigma} \times \mathbf{n}$ and $t_s = \mathbf{s} \times \boldsymbol{\sigma} \times \mathbf{n}$ in the Orz plane,

$$\begin{aligned} \Delta_h^2 t_n &= -\Delta_h^2 p + \hat{\sigma}_{zz} + [h'(r)]^2 \hat{\sigma}_{rr} - 2h'(r) \hat{\sigma}_{rz} = 0, \\ \Delta_h^2 t_s &= \left\{ 1 - [h'(r)]^2 \right\} \hat{\sigma}_{rz} + h'(r) (\hat{\sigma}_{zz} - \hat{\sigma}_{rr}) = 0. \end{aligned} \quad (31)$$

The kinematic condition prescribing the surface accumulation flux becomes

$$-\Delta_h v_n = h'(r) u - w = \Delta_h q_n = \tilde{q}, \quad (32)$$

where v_n is the normal ice velocity and \tilde{q} is the equivalent vertical flux which can be identified with equivalent vertical snowfall. In general, \tilde{q} will depend on surface elevation and location, but the later illustrations assume dependence on elevation only – dependence on location only is a simpler problem, but artificial. Equation (32) is the additional boundary condition required to determine the unknown surface $h(r)$. A prescribed temperature field incorporates a prescribed surface temperature.

The bed $z = f(r)$ is prescribed. The vectors \mathbf{s} and \mathbf{n} are defined by

$$\begin{aligned} \mathbf{n} &= \Delta_f^{-1} [f'(r), 0, -1], & \mathbf{s} &= \Delta_f^{-1} [-1, 0, -f'(r)], \\ \Delta_f &= \left\{ 1 + [f'(r)]^2 \right\}^{\frac{1}{2}}. \end{aligned} \quad (33)$$

Normal and tangential tractions t_n and t_s are given by

$$\begin{aligned} \Delta_f^2 t_n &= -\Delta_f^2 p + \hat{\sigma}_{zz} + [f'(r)]^2 \hat{\sigma}_{rr} - 2f'(r) \hat{\sigma}_{rz}, \\ \Delta_f^2 t_s &= \left\{ 1 - [f'(r)]^2 \right\} \hat{\sigma}_{rz} + f'(r) (\hat{\sigma}_{zz} - \hat{\sigma}_{rr}), \end{aligned} \quad (34)$$

and normal and tangential velocities v_n and v_s by

$$\Delta_f v_n = f'(r) u - w, \quad \Delta_f v_s = -u - f'(r) w. \quad (35)$$

The kinematic condition prescribing the normal basal melt flux, b_n , negative if freezing occurs, is

$$\Delta_f v_n = f'(r) u - w = \Delta_f b_n. \quad (36)$$

A linear sliding relation between the tangential traction and velocity is assumed, given by

$$t_s = \lambda t_n v_s, \quad (37)$$

where λ is a friction coefficient depending in general on the overburden pressure $-t_n$. The proportionality of t_s to t_n ensures bounded surface slope at the margin where the ice thickness, and overburden pressure, approach zero (Morland and Johnson, 1980). The case of no-slip gives rise to unbounded surface slope at a margin at which there is ablation in the reduced model (Morland and Johnson, 1980; Morland, 1997), which violates the expansion scheme. Figure 1 shows an ice-sheet profile with the above

conditions displayed, and gives notation for physical coordinates, velocity components and the later dimensionless variables.

4. ENHANCED REDUCED MODEL

We now introduce typical magnitudes for the physical variables so that normalized dimensionless variables can be defined. Let d_0 be a thickness magnitude and q_0 a vertical velocity magnitude, defined by a typical surface accumulation, then $\rho g d_0$ is an overburden pressure magnitude, d_0/q_0 is a flow time magnitude and q_0/d_0 is a vertical strain-rate magnitude. Typical values are adopted here,

$$d_0 = 2000 \text{ m}, \quad q_0 = 1 \text{ m a}^{-1} = 3.171 \times 10^{-8} \text{ m s}^{-1}, \quad (38)$$

then

$$\begin{aligned} \rho g d_0 &= 1.801 \times 10^7 \text{ N m}^{-2}, \\ q_0/d_0 &= 5 \times 10^{-4} \text{ a}^{-1} = 1.586 \times 10^{-11} \text{ s}^{-1}. \end{aligned} \quad (39)$$

Define

$$\begin{aligned} z &= d_0 Z, \quad h = d_0 H, \quad f = d_0 F, \quad p = \rho g d_0 P, \\ w &= q_0 W, \quad q_n = q_0 Q, \quad b_n = q_0 B, \end{aligned} \quad (40)$$

$$\mathbf{D} = (q_0/d_0) \tilde{\mathbf{D}}, \quad \hat{\boldsymbol{\sigma}} = \rho g d_0 \hat{\boldsymbol{\sigma}}, \quad (41)$$

then Z, H, P, Q, B are order unity variables, F is of order of its amplitude, κ , which may be order unity or less, and W is yet to be estimated. The viscous law (14) now becomes

$$\begin{aligned} \hat{\boldsymbol{\sigma}} &= 2\epsilon^2 \tilde{\mu} \left\{ \tilde{\mathbf{D}} + \sum_{l=1}^3 \tilde{f}(\xi_l) [\mathbf{M}^{(l)} \tilde{\mathbf{D}} + \tilde{\mathbf{D}} \mathbf{M}^{(l)} - \frac{2}{3} \text{tr}(\mathbf{M}^{(l)} \tilde{\mathbf{D}}) \mathbf{I}] \right. \\ &\quad \left. + \tilde{g}(\eta) [\tilde{\mathbf{D}} \mathbf{B} + \mathbf{B} \tilde{\mathbf{D}} - \frac{2}{3} \text{tr}(\tilde{\mathbf{D}} \mathbf{B}) \mathbf{I}] \right\}, \end{aligned} \quad (42)$$

where $\tilde{\mu}$ is defined by

$$\tilde{\mu} = \frac{1}{2} a^{-1}(T) \psi^{-1}(J), \quad (43)$$

and with the chosen parameters,

$$\epsilon^2 = \frac{\sigma_0 q_0}{\rho g d_0^2 D_0} = 2.776 \times 10^{-6}, \quad \epsilon = 0.00167. \quad (44)$$

We formally treat the product $\tilde{\mu} \tilde{\mathbf{D}}$ as an order unity quantity, since it was noted by Morland and Smith (1984) that as $a(T)$ becomes small in cold upper regions of an ice sheet, so does the strain rate. ϵ^2 is the magnitude of the dimensionless viscosity in law (42).

In the reduced model, leading order equations are developed by introducing the coordinate and variable stretchings

$$r = \epsilon^{-1} d_0 R, \quad u = \epsilon^{-1} q_0 U, \quad \omega = \epsilon^{-2} q_0 d_0^2 \Omega, \quad (45)$$

where R, U and Ω are order unity, and

$$\tilde{D}_{rr} = \frac{\partial U}{\partial R}, \quad \tilde{D}_{\theta\theta} = \frac{U}{R}, \quad \tilde{D}_{zz} = \frac{\partial W}{\partial Z}, \quad (46)$$

$$\tilde{D}_{rz} = \frac{1}{2\epsilon} \left(\frac{\partial U}{\partial Z} + \epsilon^2 \frac{\partial W}{\partial R} \right),$$

$$U = \frac{1}{R} \frac{\partial \Omega}{\partial Z}, \quad W = -\frac{1}{R} \frac{\partial \Omega}{\partial R}. \quad (47)$$

We are allowing a bed topography with modest slope δ , and with amplitude κ and span s relative to the thickness d_0 , where

$$\epsilon \ll \delta \ll 1, \quad 1 \lesssim s \lesssim 1/\delta, \quad \kappa = s\delta \lesssim 1, \quad R = \epsilon s \tilde{R}, \quad (48)$$

as treated by Morland (2000, 2001) and Cliffe and Morland (2002). Due to the bed topography, variables change with r over a dimensionless length scale s near the bed, so that \tilde{R} derivatives leave the order unchanged. Thus $F'(R)$ is order $\kappa/(\epsilon s) = \delta/\epsilon \gg 1$, and it follows from the basal melt condition (36) that W is also that order. All R derivatives of order unity variables will be of order $(\epsilon s)^{-1}$, with higher derivatives multiplied successively by this factor. We expect the surface to vary on the R scale, i.e. the scaled surface slope $H'(R) = \Gamma(R)$ to be order unity, but will allow it to be as great as the scaled bed slope $F'(R) = \beta = \mathcal{O}(\delta/\epsilon)$ in the later asymptotic expansions. For valid expansions at the margin, it must be assumed that the bed slope in a margin region must not be greater than ϵ in magnitude, and hence $F'(R)$ is order unity there. The analysis for the isotropic viscous law shows that the error of the enhanced reduced model is of order δ/s . We will now show that with the anisotropic viscous law (42) the error becomes of order δ , which is greater when $s \gg 1$.

First we must estimate the magnitudes of the dimensionless scaled stress components and their derivatives which appear in the momentum balances and boundary conditions. Note that all components of $\tilde{g}(\eta) \mathbf{B}$ never exceed unity in magnitude because of property (17) and definition (13). Immediately from (46), $\tilde{D}_{\theta\theta} = \mathcal{O}(1)$, but \tilde{D}_{rr} and \tilde{D}_{zz} are greater than order unity, so by the incompressibility condition (27) their leading order terms must be equal and opposite, namely of order $(\epsilon s)^{-1}$. This implies that where R derivatives need the factor $(\epsilon s)^{-1}$ near the bed, Z derivatives are increased by the factor κ^{-1} to reflect the topography effects, and are therefore of order ϵ/δ smaller than the corresponding R derivative. Thus, from (46),

$$\begin{aligned} \tilde{D}_{\theta\theta} &= \mathcal{O}(1), \quad \tilde{D}_{rr} = \mathcal{O}\left((\epsilon s)^{-1}\right), \\ \tilde{D}_{zz} &= \mathcal{O}\left((\epsilon s)^{-1}\right), \quad \tilde{D}_{rz} = \mathcal{O}\left((\delta \epsilon s)^{-1}\right). \end{aligned} \quad (49)$$

The relation $\tilde{D}_{zz} = \mathcal{O}(\delta \tilde{D}_{rz})$ applies throughout the depth, even when Z derivatives away from the bed leave magnitudes unchanged. Further, the order of the R derivative of W in \tilde{D}_{rz} is a factor $\delta\epsilon$ or δ^2 , near or away from the bed, respectively, of the Z derivative of U .

All components of each $\mathbf{M}^{(l)}$ are order unity. Define

$$\begin{aligned} \mathbf{A}^{(l)} &= \mathbf{M}^{(l)} \tilde{\mathbf{D}} + \tilde{\mathbf{D}} \mathbf{M}^{(l)} - \frac{2}{3} \text{tr}(\mathbf{M}^{(l)} \tilde{\mathbf{D}}) \mathbf{I}, \\ \mathbf{C} &= \tilde{g}(\eta) [\tilde{\mathbf{D}} \mathbf{B} + \mathbf{B} \tilde{\mathbf{D}} - \frac{2}{3} \text{tr}(\tilde{\mathbf{D}} \mathbf{B}) \mathbf{I}]. \end{aligned} \quad (50)$$

Note that $\mathbf{e}^{(2)} = (0, 1, 0)$, so that for $l = 1, 3$, $e_2^{(l)} = 0$, and

$$\begin{aligned} M_{rr}^{(l)} + M_{zz}^{(l)} &= \left[e_r^{(l)} \right]^2 + \left[e_z^{(l)} \right]^2 = 1, \\ \left[e_r^{(l)} \right]^2 M_{zz}^{(l)} &= \left[e_z^{(l)} \right]^2 M_{rr}^{(l)}, \quad e_r^{(l)} M_{rz}^{(l)} = e_z^{(l)} M_{rr}^{(l)}. \end{aligned} \quad (51)$$

The non-zero component of $\mathbf{A}^{(2)}$ is

$$A_{\theta\theta}^{(2)} = \frac{4}{3} \tilde{D}_{\theta\theta}, \quad = \mathcal{O}(1), \quad (52)$$

and for $l = 1, 3$ the non-zero components of $\mathbf{A}^{(l)}$ are

$$\begin{aligned} A_{rr}^{(l)} &= \frac{4}{3} M_{rr}^{(l)} \tilde{D}_{rr} - \frac{2}{3} M_{zz}^{(l)} \tilde{D}_{zz} + \frac{2}{3} M_{rz}^{(l)} \tilde{D}_{rz}, \\ A_{\theta\theta}^{(l)} &= -\frac{2}{3} M_{rr}^{(l)} \tilde{D}_{rr} - \frac{2}{3} M_{zz}^{(l)} \tilde{D}_{zz} - \frac{4}{3} M_{rz}^{(l)} \tilde{D}_{rz}, \\ A_{zz}^{(l)} &= -\frac{2}{3} M_{rr}^{(l)} \tilde{D}_{rr} + \frac{4}{3} M_{zz}^{(l)} \tilde{D}_{zz} + \frac{2}{3} M_{rz}^{(l)} \tilde{D}_{rz}, \\ A_{rz}^{(l)} &= M_{rz}^{(l)} (\tilde{D}_{rr} + \tilde{D}_{zz}) + \tilde{D}_{rz}, \end{aligned} \quad (53)$$

all dominated by \tilde{D}_{rz} with relative error of order δ by (49).

The non-zero components of \mathbf{C} are

$$\begin{aligned} C_{rr} &= \frac{2}{3}\bar{g}(\eta)(2B_{rr}\tilde{D}_{rr} - B_{\theta\theta}\tilde{D}_{\theta\theta} - B_{zz}\tilde{D}_{zz} + B_{rz}\tilde{D}_{rz}), \\ C_{\theta\theta} &= \frac{2}{3}\bar{g}(\eta)(-B_{rr}\tilde{D}_{rr} + 2B_{\theta\theta}\tilde{D}_{\theta\theta} - B_{zz}\tilde{D}_{zz} - 2B_{rz}\tilde{D}_{rz}), \\ C_{zz} &= \frac{2}{3}\bar{g}(\eta)(-B_{rr}\tilde{D}_{rr} - B_{\theta\theta}\tilde{D}_{\theta\theta} + 2B_{zz}\tilde{D}_{zz} + B_{rz}\tilde{D}_{rz}), \\ C_{rz} &= \bar{g}(\eta)((B_{rr} + B_{zz})\tilde{D}_{rz} + B_{rz}(\tilde{D}_{rr} + \tilde{D}_{zz})), \end{aligned} \quad (54)$$

where the product $\bar{g}(\eta)\mathbf{B}$ does not exceed unity in magnitude, so again all components are dominated by \tilde{D}_{rz} with relative error of order δ .

The usual scaled dimensionless deviatoric stress, $\hat{\Sigma}$, is defined by

$$\hat{\sigma} = \epsilon\hat{\Sigma}, \quad (55)$$

then from (42), (49), (50) and (52–54),

$$\begin{aligned} \tilde{D}_{rz} &= \frac{1}{2\epsilon}\frac{\partial U}{\partial Z}, \quad \hat{\Sigma}_{rz} = \tilde{\mu}c_{rz}\frac{\partial U}{\partial Z}, \\ \hat{\Sigma}_{rr} = \hat{\Sigma}_{zz} &= -\frac{1}{2}\hat{\Sigma}_{\theta\theta} = \tilde{\mu}c_{zz}\frac{\partial U}{\partial Z} = \left(\frac{c_{zz}}{c_{rz}}\right)\hat{\Sigma}_{rz}, \end{aligned} \quad (56)$$

all with relative error δ at most, where

$$c_{rz} = 1 + \bar{f}(\xi_1) + \bar{f}(\xi_3) + \bar{g}(\eta)(B_{rr} + B_{zz}), \quad (57)$$

$$c_{zz} = \frac{2}{3}[\bar{f}(\xi_1)M_{rz}^{(1)} + \bar{f}(\xi_3)M_{rz}^{(3)} + \bar{g}(\eta)B_{rz}]. \quad (58)$$

The expressions for c_{rz} and c_{zz} are order unity with relative error δ . Then the shear stress invariant, J , defined in (2), becomes

$$\begin{aligned} J &= \frac{1}{2}\vartheta \operatorname{tr}(\hat{\Sigma}^2) = \vartheta(\hat{\Sigma}_{rz}^2 + 3\hat{\Sigma}_{zz}^2) = \vartheta c \hat{\Sigma}_{rz}^2, \\ c &= 1 + 3\left(\frac{c_{zz}}{c_{rz}}\right)^2, \quad \vartheta = \frac{\rho g q_0}{\sigma_0 D_0} = 0.09, \end{aligned} \quad (59)$$

with the chosen parameters (4), (38) and (39). With the isotropic viscous law, $c_{rz} \equiv 1$, $c_{zz} \equiv 0$. By (49), \tilde{D}_{rz} is of order $(\delta\epsilon s)^{-1}$, and hence the deviatoric stress $\hat{\sigma}$ components given by (42) are of order $\epsilon/(\delta s)$, which is much smaller than unity in view of the strong inequalities (48); in fact, not greater than δ if we assert $s \gtrsim \epsilon\delta^{-2}$, which is a reasonable restriction, consistent with (48), and is assumed here. Now all the components of $\hat{\Sigma}$ are order δ/ϵ .

From (30) and (33) it follows that Δ_h and Δ_f are both unity, with maximum error δ^2 , so from (31) and (32) the surface conditions become, to lead order, neglecting terms of order δ ,

$$\Gamma = H'(R), \quad P = 0, \quad \hat{\Sigma}_{rz} = 0, \quad \Gamma U - W = Q. \quad (60)$$

Similarly, neglecting order δ terms, on the bed, from (34) and (35),

$$\begin{aligned} t_n &= -\rho g d_0 P, \quad t_s = \epsilon \rho g d_0 \Sigma_{rz}, \\ v_n &= q_0(\Gamma U - W), \quad v_s = -\epsilon^{-1} q_0 U, \end{aligned} \quad (61)$$

so that the basal boundary conditions (from (36) and (37)) become

$$\begin{aligned} \beta &= F'(R), \quad \beta U - W = B, \\ \hat{\Sigma}_{rz} &= \Lambda P U, \quad \lambda = \epsilon^2 \Lambda / q_0, \end{aligned} \quad (62)$$

and we suppose Λ is order unity or greater. The momentum

balances (29) are exactly

$$-\frac{\partial P}{\partial R} + \epsilon \frac{\partial \hat{\Sigma}_{rr}}{\partial R} + \epsilon \frac{\hat{\Sigma}_{rr} - \hat{\Sigma}_{\theta\theta}}{R} + \frac{\partial \hat{\Sigma}_{rz}}{\partial Z} = 0, \quad (63)$$

$$-\frac{\partial P}{\partial Z} + \epsilon \frac{\partial \hat{\Sigma}_{zz}}{\partial Z} + \epsilon^2 \frac{\partial \hat{\Sigma}_{rz}}{\partial R} + \epsilon^2 \frac{\hat{\Sigma}_{rz}}{R} - 1 = 0. \quad (64)$$

Since the components of $\hat{\Sigma}$ are at most of order δ/ϵ , and recalling the deduction above Equation (49) that R derivatives are not greater than a factor δ/ϵ of Z derivatives, the leading order balances of (63) and (64), neglecting terms of order δ in the former, and order δ and δ^2 in the latter, become

$$\frac{\partial \hat{\Sigma}_{rz}}{\partial Z} = \frac{\partial P}{\partial R}, \quad \frac{\partial P}{\partial Z} = -1. \quad (65)$$

Equations (60), (62) and (65) are those of the enhanced reduced model, but the fabric changes the deviatoric stress expressions (56) and the invariant J defined by (59) through the factors c_{rz} , c_{zz} and c defined by (57) and (58).

5. FLOW SOLUTION

Here we decouple the radial flow boundary-value problem defined by (55–59), (60), (62) and (65) from the fabric evolution, by assuming that the fabric through the ice-sheet domain is known; that is, $c_{rz}(r, z)$ defined by (57), $c_{zz}(r, z)$ defined by (58) and $c(r, z)$ defined by (59) are given functions. Subsequently we solve the fabric-evolution equations assuming that the velocity field is known, and then construct the coupled flow by an iteration procedure. $\tilde{\mu}$ is defined by (43) with $a(T)$ given by (7) and $\psi(J)$ by (6). Solutions of the momentum balances (65) subject to the surface conditions (60), and the invariant J defined by (59), have the simple expressions

$$\begin{aligned} P &= H(R) - Z, \quad \hat{\Sigma}_{rz} = \tau(R, Z) = -\Gamma(R)[H(R) - Z], \\ J &= \vartheta c \tau^2. \end{aligned} \quad (66)$$

Denote basal values on $Z = F(R)$ by a subscript ‘b’, then by (66) and (62),

$$\begin{aligned} P_b(R) &= H(R) - F(R) = \Delta(R), \\ \tau_b(R) &= -\Gamma(R)\Delta(R), \quad U_b(R) = -\frac{\Gamma(R)}{\Lambda[\Delta(R)]}, \end{aligned} \quad (67)$$

where $\Delta(R)$ is the ice thickness at R . From (57), (60), (67) and (47),

$$\begin{aligned} \frac{\partial U}{\partial Z} &= \frac{1}{R} \frac{\partial^2 \Omega}{\partial Z^2} = A g, \quad A(R, Z) = \frac{a}{c_{rz}}, \\ g(R, Z) &= 2\tau\psi(\vartheta c \tau^2). \end{aligned} \quad (68)$$

Integrating twice with respect to Z ,

$$\begin{aligned} U(R, Z) &= U_b(R) + g_1(R, Z), \\ g_1(R, Z) &= \int_{F(R)}^Z A(R, \bar{Z}) g(R, \bar{Z}) d\bar{Z}, \end{aligned} \quad (69)$$

$$\Omega(R, Z) = \Omega_b(R) + R[Z - F(R)]U_b(R) + R g_2(R, Z), \quad (70)$$

$$\begin{aligned} g_2(R, Z) &= \int_{F(R)}^Z g_1(R, \bar{Z}) d\bar{Z} \\ &= \int_{F(R)}^Z (Z - \bar{Z}) A(R, \bar{Z}) g(R, \bar{Z}) d\bar{Z}. \end{aligned} \quad (71)$$

Now the surface accumulation condition (60) and basal melt condition (62) with the relations (47) become

$$\begin{aligned} Z = H(R): \quad \frac{1}{R} \frac{d\Omega_s(R)}{dR} &= Q[R, H(R)], \\ Z = F(R): \quad \frac{1}{R} \frac{d\Omega_b(R)}{dR} &= B[R, F(R)], \end{aligned} \quad (72)$$

where subscript 's' denotes evaluation on the surface $Z = H(R)$. Differencing the relations in (72), and evaluating Ω_s by (70), gives

$$\Delta(R)U'_b(R) + \Delta'(R)U_b(R) + \frac{dg_{2s}}{dR} + \frac{\Delta(R)U_b(R) + g_{2s}(R)}{R} = Q - B, \quad (73)$$

where U_b is given by (67) in terms of $\Gamma(R)$ and $\Lambda(\Delta)$, and

$$U'_b(R) = \Lambda^{-2}(\Delta) [\Lambda(\Delta)\Gamma'(R) - \Lambda'(\Delta)\Delta'(R)], \quad (74)$$

$$\begin{aligned} \Gamma(R) &= H'(R), \quad \Gamma'(R) = H''(R), \\ \Delta'(R) &= H'(R) - F'(R) = \Gamma(R) - \beta(R), \end{aligned} \quad (75)$$

and g and g_{2s} depend on Γ , hence dg_{2s}/dR includes $\Gamma'(R)$. It follows that (73) is a second-order differential equation for $H(R)$.

This differential equation applies over an unknown span, the margin radius R_M , which must be determined as part of the flow solution. The subscript 'M' will denote evaluation at the margin. In section 7 the explicit second-order equation for $H(R)$ will be transformed into an equivalent system of first-order equations, and an asymptotic limit for $\Gamma'(R)$ as $R \rightarrow 0$, since $\Gamma'(R)$ is indeterminate at the divide, will be given (see (90)). As $R \rightarrow R_M$, so $\Delta \rightarrow 0$, and recalling the assumption that β is order unity near the margin, an asymptotic analysis (Morland, 1997) determines both Γ_M and Γ'_M in terms of R_M and prescribed functions evaluated at R_M ; thus

$$\begin{aligned} 2\Gamma_M &= \beta_M - \sqrt{\beta_M^2 - 4\Lambda_M(Q_M - B_M)}, \quad (76) \\ (3\Gamma_M - 2\beta_M)\Gamma'_M &= -\Lambda_M(Q'_M - B'_M) \\ &\quad + \Gamma_M\beta'_M + 2\Lambda'_M\Gamma_M(\Gamma_M - \beta_M)^2/\Lambda_M \\ &\quad - \Gamma_M(\Gamma_M - \beta_M)/R_M. \end{aligned} \quad (77)$$

Note that $\Gamma_M < \beta_M$ for positive thickness inside the margin, so the Γ'_M factor is non-zero, and Q'_M , B'_M and Λ'_M denote derivatives with respect to R , and not their given arguments. While the second-order equation could be integrated from the margin for a sequence of trial R_M , with the margin slope given by (76), until the R_M is found such that the surface slope becomes zero at $R = 0$, the indeterminacy there in Γ' is not given by the finite asymptotic limit for each incorrect trial R_M , and the numerical procedure is unstable (Morland, 1997). The stable approach (Cliffe and Morland, 2002) treats the problem as a two-point boundary-value problem with both R_M and the divide elevation $H(0) = H_D$ as unknown parameters, where the subscript 'D' denotes evaluation at $R = 0$. The differential equation is integrated from both the margin where $H = F$ and $H' = \Gamma_M$, and from the divide, $R = 0$, where $H = H_D$ and $H' = 0$, for a sequence of trial R_M and H_D until both surface elevation H and slope Γ match at a chosen interior radius. The method is described further in section 7. Once the profile $H(R)$ with R_M and H_D are determined, the velocity fields and derivatives can be determined to apply to the fabric-evolution equations.

6. FABRIC EVOLUTION

Now we assume that the domain and velocity fields and derivatives required in the evolution equations for \mathbf{B} are known. Let \tilde{t} be a dimensionless time with unit d_0/q_0 , then the kinematic relation (9) gives the non-zero relations

$$\begin{aligned} \frac{DB_{rr}}{D\tilde{t}} &= 2\tilde{D}_{rr}B_{rr} + 4\tilde{D}_{rz}B_{rz}, \\ \frac{DB_{\theta\theta}}{D\tilde{t}} &= 2\tilde{D}_{\theta\theta}B_{\theta\theta}, \\ \frac{DB_{zz}}{D\tilde{t}} &= 2\frac{\partial W}{\partial Z}B_{zz} + 2\epsilon\frac{\partial W}{\partial R}B_{rz}, \\ \frac{DB_{rz}}{D\tilde{t}} &= -\tilde{D}_{\theta\theta}B_{rz} + 2\tilde{D}_{rz}B_{zz} + \epsilon\frac{\partial W}{\partial R}B_{rr}. \end{aligned} \quad (78)$$

The relations are retained in full since some components of \mathbf{B} increase indefinitely as the stretches normal to the dominant compression increase indefinitely; we cannot set bounds. The incompressibility condition (11) is satisfied identically by using

$$B_{zz} = (1 + B_{\theta\theta}B_{zz}^2)/(B_{rr}B_{\theta\theta}), \quad (79)$$

and ignoring the evolution equation for B_{zz} . It is expected that $B_{rr} \geq B_{\theta\theta} \geq 1$, and $B_{zz} \leq 1$, or close to this situation, and both B_{rr} and $B_{\theta\theta}$ will approach infinity, and B_{zz} will approach zero, as the ice is compressed vertically as it approaches the bed, while B_{rz} , zero in the undeformed state, may be positive or negative as the ice flows through the sheet, but not greater in magnitude than B_{rr} . Numerical solution is most sensibly conducted in order unity variables, and after some trials we found that introducing the following normalized variables yielded satisfactory evolution equations,

$$\begin{aligned} \zeta_1 &= 1/B_{rr}, \quad \zeta_2 = B_{\theta\theta}/B_{rr}, \\ \zeta_3 &= B_{rz}/B_{rr}, \quad \zeta_6 = B_{zz}/B_{rr}. \end{aligned} \quad (80)$$

The three evolution equations for ζ_1 , ζ_2 and ζ_3 , by (78), are

$$\begin{aligned} \frac{D\zeta_1}{D\tilde{t}} &= -\zeta_1(2\tilde{D}_{rr} + 4\tilde{D}_{rz}\zeta_3), \\ \frac{D\zeta_2}{D\tilde{t}} &= \zeta_2(2\tilde{D}_{\theta\theta} - 2\tilde{D}_{rr} - 4\tilde{D}_{rz}\zeta_3), \\ \frac{D\zeta_3}{D\tilde{t}} &= -\zeta_3(\tilde{D}_{\theta\theta} + 2\tilde{D}_{rr} + 4\tilde{D}_{rz}\zeta_3) + 2\tilde{D}_{rz}\zeta_6 + \epsilon\frac{\partial W}{\partial R}, \end{aligned} \quad (81)$$

where, in steady flow, the material time derivative reduces to the convective terms

$$\frac{D\zeta}{D\tilde{t}} = U\frac{\partial\zeta}{\partial R} + W\frac{\partial\zeta}{\partial Z}, \quad (82)$$

for all ζ , and by the incompressibility relation (79),

$$\zeta_6 = \zeta_2^{-1}(\zeta_1^3 + \zeta_2\zeta_3^2). \quad (83)$$

7. NUMERICAL METHOD

We apply the following iteration procedure. First solve the flow problem for the profile and velocity field, and the strain-rate components and velocity derivative $\partial W/\partial R$ which are required in the fabric-evolution equations (81), for a given fabric distribution defined by functions $c_{rz}(r, z)$ and $c_{zz}(r, z)$. Then solve the fabric-evolution problem with this flow field to determine new fabric functions $c_{rz}(r, z)$ and $c_{zz}(r, z)$, which are then used to solve a new flow problem, and continue this sequence. We start by solving the flow problem with isotropic ice for which $c_{rz}(r, z) \equiv 1$ and

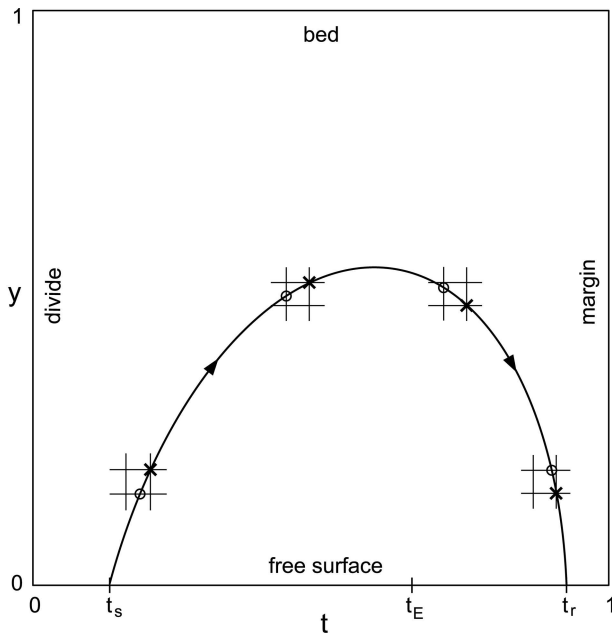


Fig. 2. Typical ice particle path in the (t, y) domain.

$c_{zz}(r, z) \equiv 0$, and continue the iteration until the final flow solution profile is sufficiently close to the previous one. To move between the two problems – a second-order ordinary differential equation with two end-point boundary conditions, on an unknown span R_M changing at each iteration, and the hyperbolic partial differential equations governing the fabric evolution – we map each ice-sheet domain in the sequence on to the same fixed domain, a unit square. Introducing new variables (t, y) by the transformations

$$\begin{aligned} R &= R_M t, & 0 \leq t \leq 1, \\ H(R) - Z &= \Delta(R)y, & 0 \leq y \leq 1, \end{aligned} \quad (84)$$

the surface $Z = H(R)$ becomes $y = 0$, the bed $Z = F(R)$ becomes $y = 1$, and the divide $R = 0$ becomes $t = 0$. The margin $R = R_M$, where the thickness $\Delta(R_M) = 0$, is expanded to $0 \leq y \leq 1$ at $t = 1$, but no depth integrals in the flow equations are required when $\Delta(R) = 0$. It is supposed that there is a single snowline in the later illustrations, at t_E , so that there is surface accumulation for $0 \leq t < t_E$ and surface melt for $t_E < t \leq 1$; that is

$$\begin{aligned} 0 \leq t < t_E: & \quad Q > 0, \\ t = t_E: & \quad Q = 0, \\ t_E < t \leq 1: & \quad Q < 0. \end{aligned} \quad (85)$$

The mapped domain and a typical ice particle path are shown in Figure 2.

With the change of variables

$$H(R) = \tilde{H}(t), \quad F(R) = \tilde{F}(t), \quad \Delta(R) = \tilde{\Delta}(t), \quad (86)$$

$$\Gamma(R) = \frac{\tilde{H}'(t)}{R_M}, \quad \beta(R) = \frac{\tilde{F}'(t)}{R_M}, \quad \Delta'(R) = \frac{\tilde{\Delta}'(t)}{R_M}, \quad (87)$$

the second-order differential equation defined by (73–75), with definition (71) for $g_2(R, Z)$, and unknown parameters R_M and H_D , can be expressed as four first-order differential

equations for $\tilde{H}(t)$, $\tilde{\Gamma}(t) = \tilde{H}'(t)$, R_M and H_D :

$$\begin{aligned} \frac{d\tilde{H}(t)}{dt} &= \tilde{\Gamma}(t), & \frac{d\tilde{\Gamma}(t)}{dt} &= G[t, \tilde{\Gamma}(t), \tilde{\Delta}(t), \tilde{\Delta}'(t), R_M], \\ \frac{dR_M}{dt} &= 0, & \frac{dH_D}{dt} &= 0, \end{aligned} \quad (88)$$

subject to the boundary conditions

$$t = 0: \quad \tilde{H} = H_D, \quad \tilde{\Gamma} = 0, \quad R_M = R_M, \quad H_D = H_D,$$

$$t = 1: \quad \tilde{H} = F(R_M), \quad \tilde{\Gamma} = R_M \Gamma_M, \quad R_M = R_M, \quad H_D = H_D,$$

where Γ_M is given by (76). The complexity lies in the surface slope derivative given by

$$\begin{aligned} &\tilde{\Delta} \left[\frac{1}{\Lambda} + \tilde{\Delta}^2 J_1 \right] G \\ &= -R_M^2 (Q - B) - \tilde{\Gamma} \tilde{\Delta}' \left[\frac{1}{\Lambda} - \frac{\tilde{\Delta} \Lambda'(\tilde{\Delta})}{\Lambda^2} + \tilde{\Delta}^2 (J_1 + 2I_1) \right] \\ &\quad - \frac{\tilde{\Gamma} \tilde{\Delta}^3}{R_M} \left(\tilde{\Gamma}^2 \tilde{\Delta}^2 J_C + R_M^2 K_1 \right) - \frac{\tilde{\Gamma} \tilde{\Delta}}{t} \left[\frac{1}{\Lambda} + \tilde{\Delta}^2 I_1 \right], \end{aligned} \quad (89)$$

where

$$h_1(t) = 2 \int_0^1 A(R, Z) \psi(J) y^2 dy,$$

$$J_1(t) = 4\vartheta \int_0^1 A(R, Z) c(R, Z) \psi'(J) y^4 dy,$$

$$K_1(t) = 2 \int_0^1 \frac{\partial A}{\partial R}(R, Z) \psi(J) y^2 dy,$$

$$J_C(t) = 2\vartheta \int_0^1 A(R, Z) \psi'(J) \frac{\partial c}{\partial R}(R, Z) dy$$

and

$$J_1(t) = h_1(t) + R_M^{-2} \tilde{\Gamma}^2 \tilde{\Delta}^2 J_1(t).$$

The integrand functions of (R, Z) must be transformed to (t, y) dependence before integration, and in particular the partial derivative $\partial c / \partial R$ at constant Z must be expressed in terms of partial derivatives with respect to t and y , then the latter is integrated out by parts.

The expression (89) for G is indeterminate as $t \rightarrow 0$ at the divide, and as $t \rightarrow 1$ when $\tilde{\Delta} \rightarrow 0$ at the margin. The latter asymptotic limit is simply $G_M = R_M^2 \Gamma_M$, where Γ_M is given by (76). The former asymptotic limit is

$$\tilde{\Delta}_D \left[\frac{1}{\Lambda_D} + \tilde{\Delta}_D^2 J_1(0) \right] G_D = -\frac{1}{2} R_M^2 (Q_D - B_D). \quad (90)$$

The velocity fields U and W are then given by (47), and the strain-rate components, required by the fabric-evolution equations (81), are given by (46) and (56) with Ω given by (70). These involve integrals from y_j to 1 at t_i for each mesh point (t_i, y_j) . In addition, (81) requires the velocity derivative $\partial W / \partial R$ at constant Z , which is determined numerically by cubic expansions of W in the t and y directions using values at (t_i, y_j) and three adjacent points.

A uniform mesh is placed on the square with n intervals of length h_t in the t direction, and m intervals of length h_y in the y direction, defining mesh points (t_i, y_j) , ($i = 0, \dots, n$; $j = 0, \dots, m$). Given that the fabric-evolution solution has determined c_{rz} , c_{zz} and hence c , at each mesh point (t_i, y_j) , the required t derivatives are obtained by cubic interpolation based on four adjacent mesh points in the t direction. For the flow problem, the depth integrations are performed using a trapezoidal approximation, with error h_y^3 , and the differential equations (88) are solved using a second-order Runge–Kutta

scheme with error h_t^3 . Newton's root-finding method is used to determine the parameters R_M and H_D which match the surface elevation and slope at the interior point $t = 0.5$. Using double precision, the matching error for all the later examples was initially of order 10^{-8} , retaining eight decimal places in R_M and H_D , but the final solutions were obtained retaining only six decimal places. The iteration between flow and fabric evolution was continued until a measure of the change from the previous flow solution defined by

$$er = \max\left(\frac{[R_M]}{R_M}, \frac{[H_D]}{H_D}, \frac{\sum_{i=0}^{n-1} [\tilde{\Delta}(t_i)]}{n\tilde{\Delta}_D}\right) \quad (91)$$

was acceptably small, where $[]$ denotes the jump from the previous solution in the iteration sequence. In all the later examples er did not exceed order 10^{-5} , and the rate of decrease in the later stages suggested that a further iteration would have yielded a much smaller value, so this final solution can be expected to change less than 10^{-5} with a further iteration.

Figure 2 shows a typical particle path in the (t, y) domain, starting from an accumulation point on the surface $(t_s, 0)$, where $0 < t_s < t_E$, and returning to the surface at an ablation point $(t_r, 0)$ where $t_E < t_r < 1$. Let $\zeta(R, Z) = \tilde{\zeta}(t, y)$ for all ζ , and let s denote arc length on a particle path in the (t, y) domain defined by $t = \tilde{\zeta}_4(s)$, $y = \tilde{\zeta}_5(s)$, for which

$$\begin{aligned} \frac{dy}{dt} &= \frac{1}{U\tilde{\Delta}} [U(\tilde{\Gamma} - y\tilde{\Delta}') - R_M W] = y_d, \\ \frac{d\tilde{\zeta}_4}{ds} &= \frac{1}{\sqrt{1 + y_d^2}}, \quad \frac{d\tilde{\zeta}_5}{ds} = \frac{y_d}{\sqrt{1 + y_d^2}}. \end{aligned} \quad (92)$$

The fabric-evolution equations (81), with the relation (82), now become

$$\begin{aligned} \frac{d\tilde{\zeta}_1}{ds} &= -\nu\tilde{\zeta}_1(2\tilde{D}_{rr} + 4\tilde{D}_{rz}\tilde{\zeta}_3), \\ \frac{d\tilde{\zeta}_2}{ds} &= \nu\tilde{\zeta}_2(2\tilde{D}_{\theta\theta} - 2\tilde{D}_{rr} - 4\tilde{D}_{rz}\tilde{\zeta}_3), \end{aligned} \quad (93)$$

$$\begin{aligned} \frac{d\tilde{\zeta}_3}{ds} &= -\nu\tilde{\zeta}_3(\tilde{D}_{\theta\theta} + 2\tilde{D}_{rr} + 4\tilde{D}_{rz}\tilde{\zeta}_3) + 2\tilde{D}_{rz}\tilde{\zeta}_6 + \epsilon \frac{\partial W}{\partial R}, \\ \nu &= \frac{R_M}{U\sqrt{1 + y_d^2}}. \end{aligned} \quad (94)$$

(92–94) are five ordinary differential equations for $\tilde{\zeta}_1$ to $\tilde{\zeta}_5$, subject to the initial surface conditions at $s = 0$ on $y = 0$, $t = t_s$ where $0 \leq t_s \leq t_E$,

$$\tilde{\zeta}_1 = 1, \quad \tilde{\zeta}_2 = 1, \quad \tilde{\zeta}_3 = 0, \quad \tilde{\zeta}_4 = t_s, \quad \tilde{\zeta}_5 = 0.$$

Values of $\tilde{\zeta}_1$ to $\tilde{\zeta}_3$, and in turn the values of c_{rz} , c_{zz} , c and their derivatives, must be determined at each mesh point (t_i, y_j) , where they are required for the subsequent flow solution.

The divide $t = 0$ is a particle path with $s = y$, but as $t \rightarrow 0$, so does U , $\tilde{\Gamma}$ and $\tilde{\Delta}'$, and hence $y_d \rightarrow \infty$ when $W \neq 0$, but

$$\begin{aligned} t \rightarrow 0: \quad U\sqrt{1 + y_d^2} &\rightarrow Uy_d \rightarrow -R_M W / \tilde{\Delta}_D, \\ \nu &\rightarrow -\tilde{\Delta}_D / W \quad \text{for } W \neq 0, \end{aligned} \quad (95)$$

and ν is bounded. On $t = 0$, $\tilde{D}_{rr} = \tilde{D}_{\theta\theta}$ (positive), $\tilde{D}_{rz} = 0$, and we suppose the bed slope does not exceed order ϵ near the divide, so the derivative $\partial W / \partial R$ is order unity there.

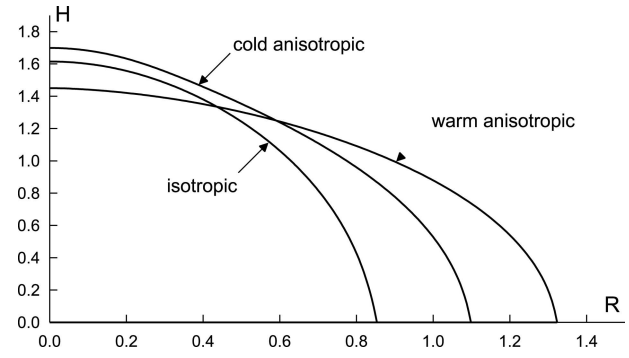


Fig. 3. Free surface profiles for isotropic, cold and warm ice; for flat bed.

Then, neglecting the term of order ϵ , the three non-trivial equations for $\tilde{\zeta}_1$ to $\tilde{\zeta}_3$ on the divide become

$$\frac{d\tilde{\zeta}_1}{dy} = -2\nu\tilde{D}_{rr}\tilde{\zeta}_1, \quad \frac{d\tilde{\zeta}_2}{dy} = 0, \quad \frac{d\tilde{\zeta}_3}{dy} = -3\nu\tilde{D}_{rr}\tilde{\zeta}_3, \quad (96)$$

which can be integrated numerically. However, if $W \rightarrow 0$ as well, then y_d is indeterminate, as is the case in our later examples which assume zero basal melting, and hence $W = 0$ at the base of the divide. However, the ν limit given in (95) is still the correct asymptotic behaviour, the other terms of y_d being smaller, and since \tilde{D}_{rr} is positive, then \tilde{D}_{zz} is negative by incompressibility, and hence W behaves like $-(1 - y)$ and ν like $(1 - y)^{-1}$, positive, as $y \rightarrow 1$. Immediately $\tilde{\zeta}_2 \equiv 1$, so $B_{\theta\theta} \equiv B_{rr}$, $\tilde{\zeta}_1$ behaves like a positive power of $(1 - y)$, and $\tilde{\zeta}_3$ like a larger positive power of $(1 - y)$, so $B_{rr} \rightarrow \infty$, $B_{rz} \rightarrow 0$ and $B_{zz} \rightarrow 0$, by incompressibility. On the divide, the unit vectors $\mathbf{e}^{(l)}$ are along the coordinate axes so $b_1 = B_{rr}$, $b_2 = B_{\theta\theta}$, $b_3 = B_{zz}$, and hence, by (13), $\xi_1 \rightarrow \infty$, $\xi_3 \rightarrow -\infty$, $\eta \sim K \sim 2b_1 \rightarrow \infty$, and by (12) each $M_{rz}^{(l)}$ is zero. Thus by (21), (57) and (58),

$$\begin{aligned} c_{rz} &\rightarrow 1 + \bar{f}(\infty) + \bar{f}(-\infty) + \frac{1}{2}\bar{G}(\infty) = \frac{1}{2}(3A - S), \\ c_{zz} &\rightarrow 0. \end{aligned} \quad (97)$$

This asymptotic limit is approached smoothly by the numerical integration to the last point before the bed $y = 1$. The bed is also a particle path when $B = 0$, but direct numerical integration in $s = t$ from the margin is not possible because of the singular, but not explicit, behaviour of ν there.

The first approach was to integrate the five differential equations for $\tilde{\zeta}_1$ to $\tilde{\zeta}_5$ from the surface mesh points on $(0, t_E)$ using a second-order Runge–Kutta method with integration interval h_t , until the closest point to $(t_r, 0)$ was reached. Values at each mesh point were then interpolated by using nine or ten closest path points in both rectangular and polar expansions. It was found that all such interpolations became erratic in some neighbourhoods of the bed, $y = 1$, which we believe is because the paths become parallel and bunch close together there.

An accurate method is to integrate the path equations (92) for $\tilde{\zeta}_4$ and $\tilde{\zeta}_5$ backwards from each mesh point (t_i, y_j) , to determine the corresponding start value t_s on $y = 0$. The final value is determined by using repeated tangent extrapolations over shorter intervals from the last point before the line $y = 0$ is crossed, stopping when the last interval is less than 10^{-6} . Then all five evolution equations (92) and (93) are integrated

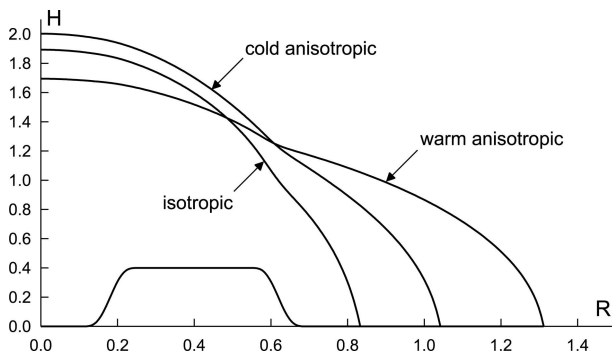


Fig. 4. Free surface profiles for isotropic, cold and warm ice on the illustrated hump bed.

forward from $(t_s, 0)$ to (t_i, y_i) . The high accuracy is confirmed by the accurate return to (t_i, y_i) . With the necessarily fine mesh using second-order integration routines, computing time for the reverse and return integrations for the large number of mesh points is extremely large (many hours on an Apple G4), and must be repeated many times for the iteration between evolution and flow. An alternative strategy was therefore devised. The backward integration from each (t_i, y_i) was performed to determine the point (t_0, y_0) where the path first crossed a previous mesh line: $t = t_{i-1}$ or $y = y_{j-1}$ or $y = y_{j+1}$; the four possibilities are shown in Figure 2 with typical mesh points denoted by a cross and the previous mesh line intersections by circled points. The above tangent extrapolation method was again used to determine accurate (t_0, y_0) . The values of $\zeta_1, \zeta_2, \zeta_3$ at (t_0, y_0) are determined by quadratic interpolation using values at three appropriate adjacent mesh points, then the five equations are integrated forward to (t_i, y_i) . The different possible configurations for the location of the point (t_0, y_0) , which require known values at different sets of adjacent mesh points, complicates the procedure for covering the domain to provide all required values for the interpolations, but this strategy has proved very fast and accurate. The accuracy is confirmed by applying the full reverse and return integrations to selected sets of mesh points: adjacent to the divide, adjacent to the bed, and in the ablation zone of the surface; in particular the bed neighbourhood could be expected to yield the worst errors. In all the later examples, it was only at a few places in the bed, towards the margin, that significant differences arose, up to a few per cent in small zones, but these should make little difference to the depth integrals in the flow equations. The solution for mesh points on the bed was obtained by integrating the five differential equations from a surface point $(10^{-7}, 0)$ for which the particle hugs the divide, bed and expanded margin line, and linearly interpolating

Table 1. Flat-bed parameters

	Isotropic	Cold	Warm
H_D	1.61488	1.69916	1.45001
R_M	0.85329	1.09837	1.32322
R_E	0.75300	0.95888	1.06420
$(c_{rz})_{DB}$	1.0	4.4	0.4375
$(c_{rz})_M$	1.0	0.87655	0.15649

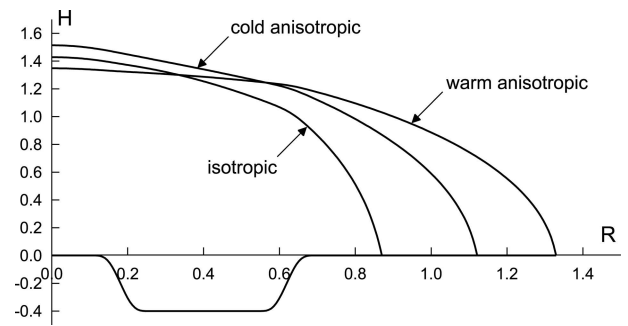


Fig. 5. Free surface profiles for isotropic, cold and warm ice on the illustrated basin bed.

between values at integration points t on either side of t_i . The final values at $(1, 0)$ are used for the complete line $t = 1$, $0 \leq y \leq 1$, since this is the expanded margin.

8. ILLUSTRATIONS

A temperature distribution used by Morland (1997) is adopted,

$$\begin{aligned} \bar{T} = & -0.8H + 0.5(H - Z) \\ & - 0.125\Delta \left[\Delta(H - Z) - 0.5(H - Z)^2 \right], \\ = & -0.8H + 0.5\Delta y \left[1 - 0.125\Delta^2(2 - y) \right], \end{aligned} \quad (98)$$

where H and Δ denote $H(R)$ and $\Delta(R)$, respectively, which depends on surface elevation and depth below the surface. The corresponding thermal boundary conditions are

$$\begin{aligned} Z = H(R): \quad \bar{T}_s &= -0.8H(R), \\ Z = 0: \quad \frac{\partial \bar{T}}{\partial Z} &= -0.5, \end{aligned} \quad (99)$$

with the realistic properties that the surface temperature decreases at a rate of 0.8 K per 100 m rise, and that there is a uniform heat flux into the base equivalent to a temperature gradient of 0.5 K per 100 m, and the Laplacian of T , arising in the energy balance, is bounded.

The surface accumulation/ablation distribution adopted is an elevation-dependent example with large margin ablation, $-Q_M$, used by Morland (1997),

$$\begin{aligned} Q &= 0.5 - 6.5 \exp(-4H), \\ Q_M &= -6, \quad Q \rightarrow 0.5 \text{ as } H \rightarrow \infty, \end{aligned} \quad (100)$$

with a decay height scale $H = 0.25$ corresponding to $h = 500$ m. The equilibrium height (snowline) where $Q = 0$ is at $H = 0.64$ corresponding to $h = 1280$ m. Cliffe and Morland (2004) have investigated the dynamic stability

Table 2. Hump-bed parameters

	Isotropic	Cold	Warm
H_D	1.89327	2.00287	1.69473
R_M	0.83302	1.04195	1.31155
R_E	0.73223	0.90962	1.14105
$(c_{rz})_{DB}$	1.0	4.4	0.4375
$(c_{rz})_M$	1.0	0.69781	0.14619

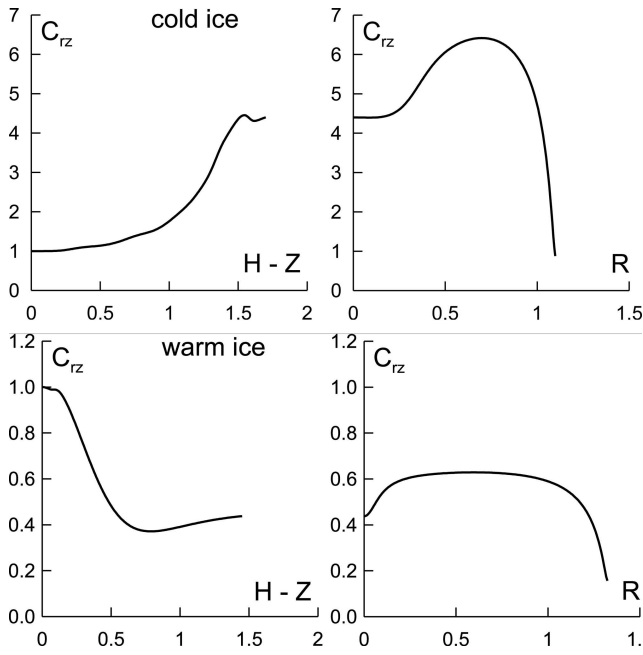


Fig. 6. Distributions of the viscosity factor, c_{rz} , down the divide (as a function of $H-Z$) and along the bed (as a function of R) for cold and warm ice; for flat bed.

of radial flow for linearly viscous ice with varying weighting of the accumulation dependence on elevation and location, and demonstrate in particular that dependence on elevation alone is unstable. However, direct solution of the steady flow equations with this function has always proved numerically stable, and it describes a simple, physically plausible distribution. The basal melting $B \equiv 0$, and a constant friction coefficient $\Lambda \equiv 25$, are adopted in all the examples presented.

We compare solutions for a flat bed, for a bed with a single symmetric hump of amplitude 0.4, corresponding to 800 m, maximum slope $\delta = 0.01$, and slope span $s = 40$, corresponding to 80 km, centred at $R_c = 0.4$, corresponding to $r_c = 479$ km, and for a single symmetric basin which is the image of the above hump. All three cases are described by the smooth bed form

$$F(R) = \kappa \begin{cases} 0 & \text{if } 0 \leq R < R_c - 2e, \\ \bar{F}(\chi) & \text{if } R_c - 2e \leq R \leq R_c - e, \\ 1 & \text{if } R_c - e < R < R_c + e, \\ \bar{F}(\bar{\chi}) & \text{if } R_c + e \leq R \leq R_c + 2e, \\ 0 & \text{if } R > R_c + 2e, \end{cases} \quad (101)$$

with

$$\chi = (R - R_c + 2e)/e, \quad \bar{\chi} = (R_c + 2e - R)/e,$$

Table 3. Basin-bed parameters

	Isotropic	Cold	Warm
H_D	1.42820	1.51391	1.34855
R_M	0.87001	1.12128	1.32933
R_E	0.76908	0.98000	1.15784
$(c_{rz})_{DB}$	1.0	4.4	0.4375
$(c_{rz})_M$	1.0	1.00120	0.15775

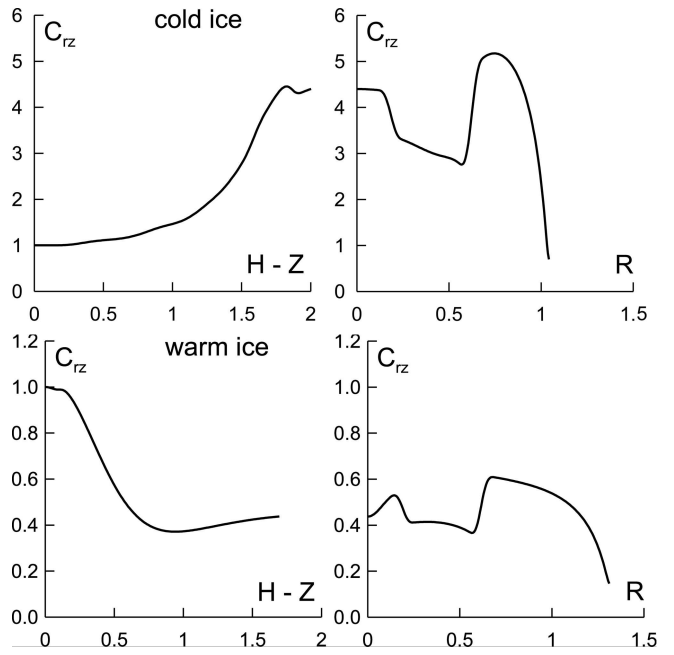


Fig. 7. Distributions of the viscosity factor, c_{rz} , down the divide (as a function of $H-Z$) and along the bed (as a function of R) for cold and warm ice; for hump bed.

where the R span of the slope sections is e , and of the flat section is $2e$, and $\bar{F}(\chi)$ is a monotonic polynomial

$$\bar{F}(\chi) = \chi^4(35 - 84\chi + 70\chi^2 - 20\chi^3). \quad (102)$$

$F(R)$ and its first three derivatives are continuous at $R_c - 2e$, $R_c - e$, $R_c + e$ and $R_c + 2e$, and $F(R)$ has a maximum slope at $\chi = 0.5$ and $\bar{\chi} = 0.5$ where

$$F'(R) = -\frac{35\kappa}{16e} = -\frac{\delta}{\epsilon} \quad \text{if } e = \frac{35}{16}\epsilon s = 0.146 \quad (103)$$

with the chosen parameters, corresponding to a maximum

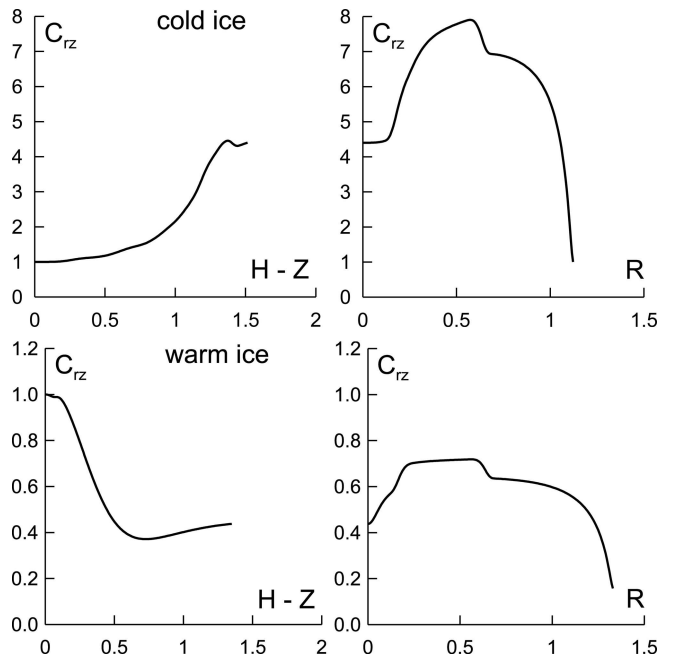


Fig. 8. Distributions of the viscosity factor, c_{rz} , down the divide (as a function of $H-Z$) and along the bed (as a function of R) for cold and warm ice; for basin bed.

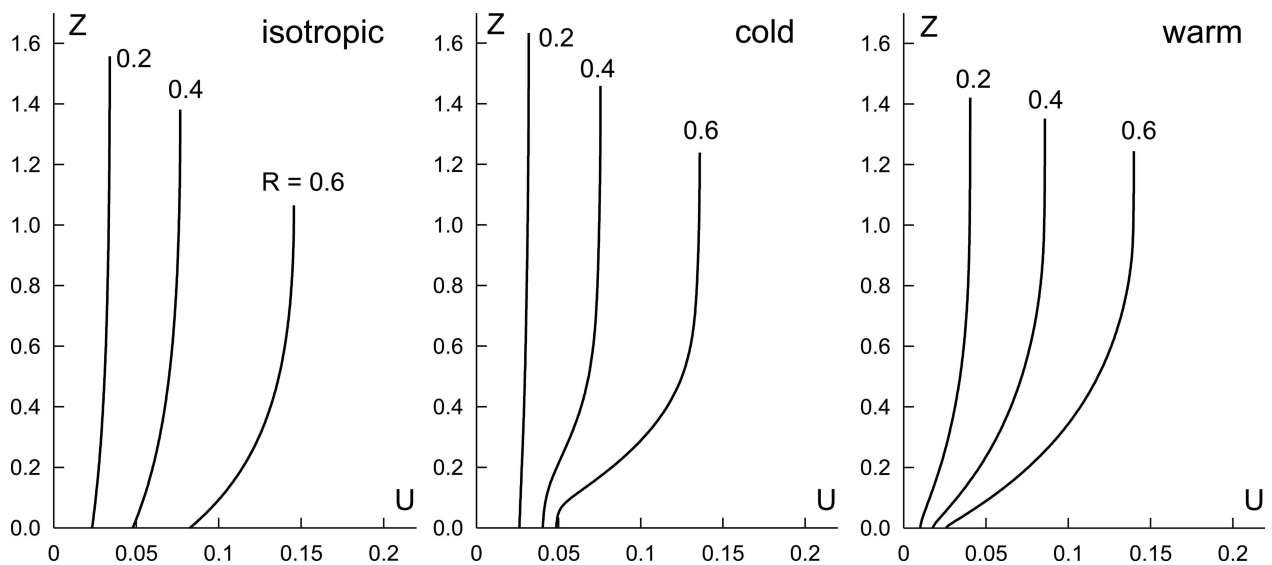


Fig. 9. Horizontal velocity depth profiles at $R = 0.2$, $R = 0.4$ and $R = 0.6$, for isotropic, cold and warm ice; for flat bed.

physical slope $\delta = 0.01$ and a hump/basin spanning 174 km. The flat, hump and basin topographies are given, respectively, by $\kappa = 0, 0.4$ and -0.4 .

The solution computations were performed on a mesh with $n = m = 1000$ so that $h_t = h_y = 0.001$. In all three cases, the fabric parameter c_{zz} remained very small, not exceeding a few per cent, so the parameter c in (59) remained close to unity. The fabric influence on the flow is therefore mainly through the fabric parameter c_{rz} , the viscosity factor arising in the $\hat{\Sigma}_{rz}$ relation (56), and defined by (57). We now present comparisons of the isotropic-ice, cold-ice, and warm-ice solutions for the three bed topographies. Tables 1–3 show H_D , R_M , R_E , $(c_{rz})_{DB}$ and $(c_{rz})_M$, where R_E is the scaled radius where $Q(H)$ is zero, and $(c_{rz})_{DB}$ denotes the value at the base of the divide, here $R = 0$, $Z = 0$, given by the asymptotic limit (97), for the flat, hump and basin beds. At the base of the divide, where the vertical compression is large, $(c_{rz})_{DB}$ has the same limit values for all three topographies, but this greatly exceeds unity for cold

ice, and is significantly less than unity for warm ice, associated with the limit compression factor A , given in (20), exceeding unity for cold ice and less than unity for warm ice. The viscosity factor at the margin, $(c_{rz})_M$, decreases from its unit isotropic value for the cold ice, and more dramatically for the warm ice, in the flat- and hump-bed cases, but in the basin-bed case it still decreases dramatically for warm ice, but is close to unity for cold ice. For all three bed forms, the margin span R_M increases from isotropic to cold to warm ice, while the divide height H_D increases slightly then decreases more for the same sequence, but, as expected, increases from basin to flat to hump beds.

Figures 3–5 show the bed and surface profiles for the isotropic, cold and warm ice, for the flat, hump and basin beds, respectively. These illustrate the distinct, and significant, effects of the two forms of fabric evolution treated, particularly on the span R_M . For a given R_M and fabric law, the divide height H_D is essentially governed by the steady-state assumption, that there is no net flux in or out of the sheet.

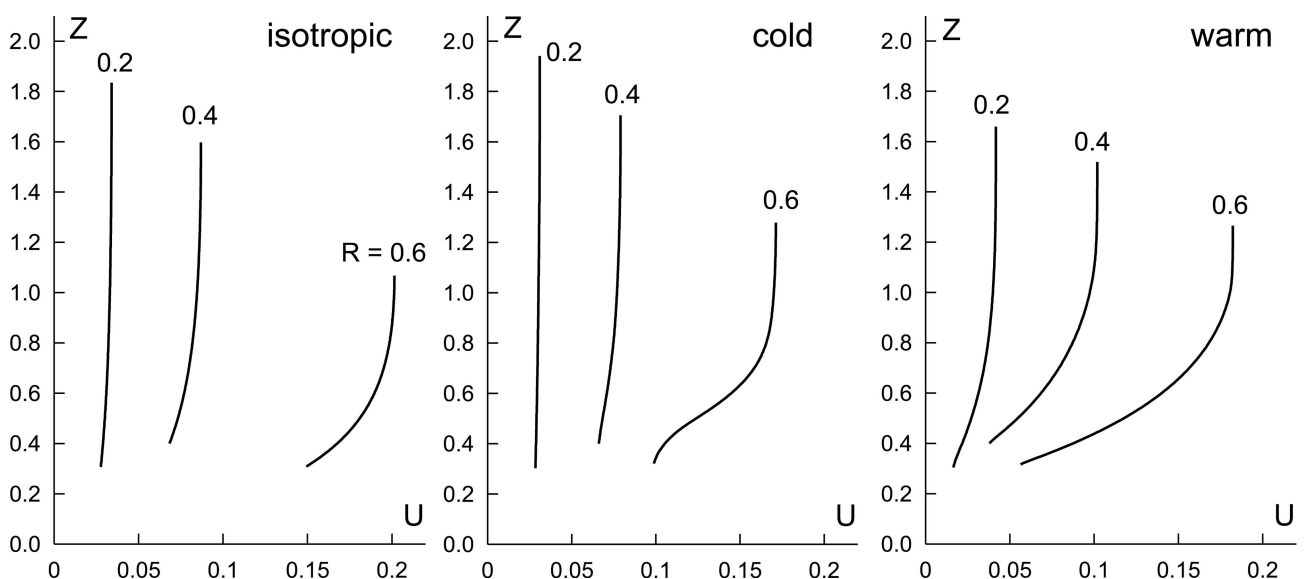


Fig. 10. Horizontal velocity depth profiles at $R = 0.2$, $R = 0.4$ and $R = 0.6$, for isotropic, cold and warm ice; for hump bed.

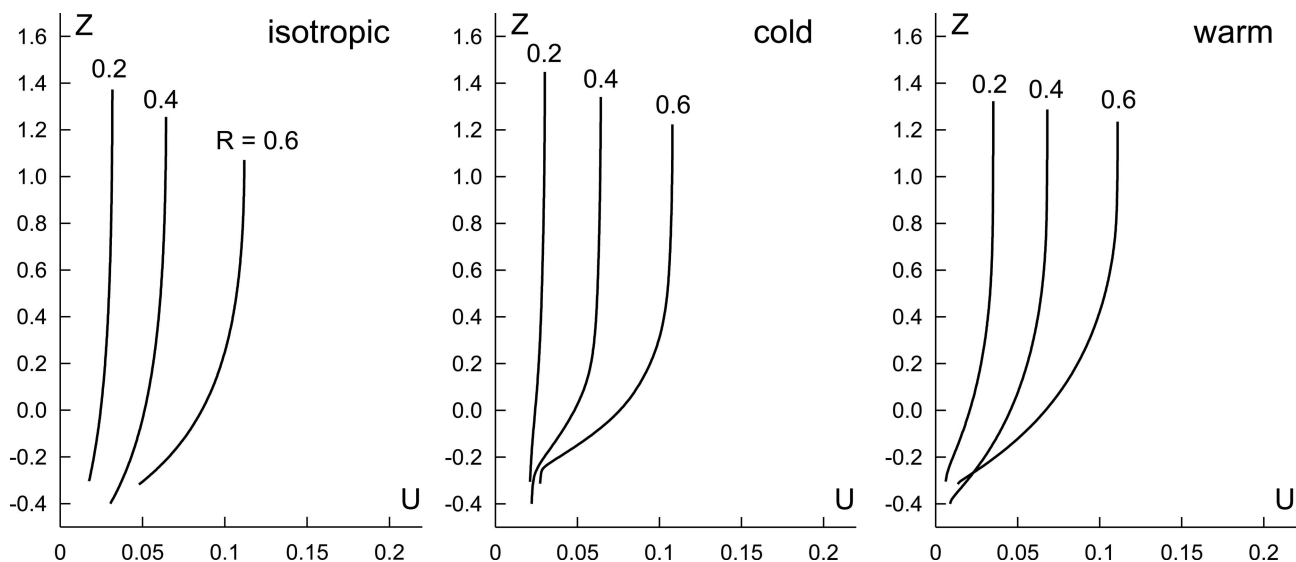


Fig. 11. Horizontal velocity depth profiles at $R = 0.2$, $R = 0.4$ and $R = 0.6$, for isotropic, cold and warm ice; for basin bed.

The viscosity factor c_{rz} is identically unity for the isotropic ice. Figure 6 shows the distribution of c_{rz} , first down the divide as a function of $H - Z$, then along the bed as a function of R , for cold and warm ice, in the flat-bed case. This gives a measure of how the fabric is affecting the shearing rate of the ice, down the symmetry axis and along the bed. Figure 7 shows the same for the hump bed and Figure 8 for the basin bed. There is a significant effect from the bed topographies. While c_{rz} for the warm ice is mainly decreasing along these two boundaries, consistent with the increase of span R_M from the isotropic span, the effect of decreasing c_{rz} along the bed, and in the sheet interior, for the cold ice, must offset the increase down the divide, since R_M is again greater than the isotropic span for each bed form, though less than the warm span.

Figure 9 shows, for the flat bed, the distributions of the horizontal scaled velocity, U , with height at locations $R = 0.2$, $R = 0.4$, $R = 0.6$ for isotropic, cold and warm ice. Recall that the hump/basin topographies are centred at $R_c = 0.4$. The effects of fabric are increased with distance from the divide as expected, particularly near the bed. Figure 10 shows the same for the hump bed, and Figure 11 for the basin bed, with similar effects, and with increased changes near the bed due to the topographies.

9. CONCLUSIONS

An enhanced reduced model for steady radially symmetric flow of an ice sheet with fabric evolution, over bed topographies with a modest maximum slope, δ , has been derived, where $\epsilon \ll \delta \ll 1$ and ϵ is the surface slope magnitude. It is described by the leading order balances of the mass and momentum equations, boundary conditions and the constitutive law for the ice governing the fabric (induced anisotropy) evolution, with errors of order δ .

Numerical solutions for a flat bed, a bed with a single symmetric hump and a bed with a single symmetric basin have been constructed, for two forms of the fabric evolution, described as cold ice and warm ice. Tables of the key parameters – divide height, margin radius, equilibrium-line

radius and the fabric-induced viscosity factor – are presented for the isotropic, cold and warm ice for each of the bed forms. The radial span, margin radius, is seen to be strongly influenced by the induced fabric. Figures illustrate the distinct ice-sheet profiles, the distribution of the fabric-induced viscosity factor down the divide and along the bed, and the distributions with height of the horizontal velocity, for the different ice laws and bed topographies. All illustrate the significant effect of fabric evolution compared to the conventional isotropic ice model.

The adopted fabric-evolution model does not account for possible fabric weakening due to migration recrystallization occurring at high (near-melting) temperature or high strain rate, which may arise in thin zones near an ice-sheet bed. Since bed conditions have a major influence on the flow and profile, such weakening could make a significant difference to the solutions and conclusions. If, however, such zones are not extensive, but confined to limited areas of the bed, then the magnitudes of the effects derived here may still apply. To reach a firmer conclusion, a constitutive model which realistically describes such weakening effects must first be established and incorporated in the ice-sheet flow equations, and then solutions for simple flow configurations obtained.

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