

A frequency lock-in mechanism in the interaction between wind and crop canopies

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The interaction between wind dynamics and the waving of crop canopies is explored. On-site experiments with wheat and alfalfa fields allow us to quantify the motion of a large set of plants subject to wind using an image correlation technique. The coherent part of the waving motion is extracted by a bi-orthogonal decomposition of the spatio-temporal velocity field of the crop surface. It is shown that the corresponding space and time features cannot be explained using predictions from the mixing layer analogy of wind above canopies, which is the most common model for perturbations in this environment. We show that the plant bending stiffness plays an important role in the frequency and wavelength selection for the coherent motion of the canopy. A fully coupled model, where the wind fluctuations and the plant dynamics interact through a drag term, is then proposed. This model allows us to demonstrate a lock-in mechanism, similar in principle to what is found in vortex-induced vibration, whereby the frequency of the instability deviates from its expected value when approaching the natural frequency of the oscillating medium. This finding is then compared to data from on-site experiments,

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and good agreement, in both frequency and wavelength of the propagating patterns observed on the canopy surface, is shown.

1. Introduction

Wind-induced motion of crop canopies may result in crop damage, namely the phenomenon of lodging (or windthrow) which is responsible for massive loss in grain yield worldwide (Baker 1995). Moreover, wind-induced motion is known to influence plant growth and biomass production. This latter effect is referred to as thigmomorphogenesis (Jaffe 1973), and its practical application in agronomy has only recently been demonstrated (Moulia & Combes 2004). For both lodging and thigmomorphogenetic analyses, an accurate description of the strong coherent motion of the crops under wind and a better understanding of the coupling between wind and canopy dynamics is necessary.

Wind turbulence within and over plant canopies has long been viewed as a perturbed version of the turbulence present in the atmospheric boundary layer. However, over the last three decades, our knowledge of canopy turbulence has steadily advanced, as reported in the two reviews by Raupach & Thom (1981) and Finnigan (2000). This was motivated by such problems as the transport of pollen and other particles, CO₂, heat and vapour exchanges between vegetation and the atmosphere including their role in canopy microclimates, as well as wind damage to forests and crops. One of the major developments has been the recognition that wind turbulence is dominated by large coherent structures that scale with the canopy height. Single-point statistics of turbulence in the roughness sub-layer, occupied by the canopy and the air layer just above, differ in many aspects significantly from those in the surface layer: the mean velocity profile is inflected at the canopy top (Figure 1), second-order moments are strongly inhomogeneous with

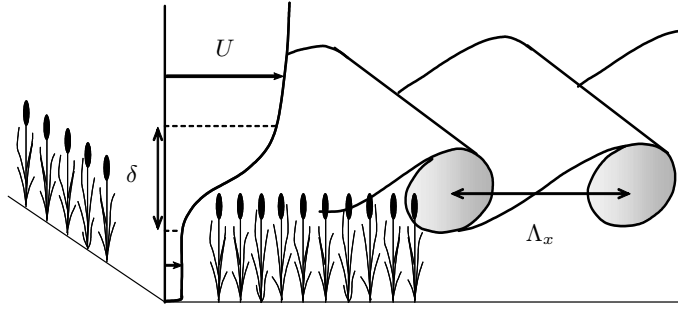


FIGURE 1. Sketch of the mixing layer instability of wind over plant canopies, adapted from Finnigan (2000), where δ is the vorticity thickness and Λ_x the dominant streamwise length scale.

respect to height, skewness and correlation coefficients are large, and velocity moments are proportional to a unique length and time scale throughout the layer (Finnigan 2000). Comparison with the statistics and instability modes of a plane mixing layer shows that the latter, rather than the boundary layer, is the appropriate model for canopy flow and that the dominant vortices result from an inviscid instability associated with the inflection of the mean velocity profile, see Raupach, Finnigan & Brunet (1996). For canopies ranging from grass to forests, the dominant streamwise length scale Λ_x of canopy turbulence has been shown by Raupach *et al.* (1996) to be controlled by a unique shear length scale, proportional to the canopy height, and equivalent to the vorticity thickness δ commonly used to describe the inflection of mixing layer profiles (Huerre 2000), see Figure 1. Following the work of Raupach *et al.* (1996) on terrestrial canopies, a recent study by Ghisalberti & Nepf (2002) has shown that the mixing layer model was also applicable to the flow through and above submerged aquatic vegetations.

The wave-like motion of crops on windy days, called *honami* (Inoue 1955), provides striking visualisations of the propagating coherent structures of wind resulting from the above-mentioned mixing layer type instability, if one assumes that the canopy simply behaves as a passive vibrating medium excited by the wind fluctuations. However, several

aspects of the wind dynamics and its coupling with the plant canopies remain unclear. First, it is surprising that vortex structures resulting from a Kelvin-Helmholtz instability may form in the wind over canopies in the presence of naturally high levels of noise, whereas convective mixing layers are known to be highly sensitive to external noise (Huerre 2000). The instability over plant canopies seems to be less sensitive to noise than classical shear layer instabilities. It has been suggested by Finnigan (2004) that the plant motion may affect the flow dynamics and promote vortex roll-up, through a mechanism that remains to be clarified. Second, the dominant frequencies measured in the wind over waving wheat were found to closely match the free vibration frequency of the wheat plants (Finnigan (1979)). This is incompatible with the mixing layer model which predicts a dominant frequency set by the vorticity thickness of the mean wind profile. This therefore suggests a non-negligible influence of the plant vibrations on the flow dynamics. These two features, namely, the low sensitivity to noise and the selection of a dominant frequency, both suggest that the canopy does not behave as a passive vibrating medium but rather plays a role in the instability itself.

Consequently it is necessary to study wind flow over canopies and wind-induced motion of plants in a fully coupled way. Despite intensive field studies of wind flow over canopies, only few qualitative information (Finnigan 1979), and no quantitative data, are available regarding the coherent motion of plant canopies. The experimental technique recently developed by Py *et al.* (2005) allows the characterization of the spatio-temporal motion of crops subject to wind under field conditions. In the first part of this paper, Section 2, we present experimental results of in-situ measurement of the motion of two crops under wind. Then, in order to explain the features revealed by the experiments, a model is proposed in Section 3 that couples wind flow and canopy motion. A temporal linear stability analysis allows us to compute the characteristics of the coupled instability

underlying both the coherent structures of wind and the waving of the canopy, and an insight into the wind-crop coupling is gained. In Section 4, the predictions of this model are compared to the experimental results of Section 2.

2. Experimental characterisation of the waving of crop canopies

The goal of the experiments described below is to quantitatively describe the global motion of crop canopies under wind and, more specifically, to identify the wave-like motion that can be observed on crops on windy days. The spatio-temporal features of these waves are investigated with the aim of understanding the underlying instability mechanism.

2.1. *Experimental approach*

For completeness, we recall the main features of the experimental technique used to measure the motion of waving crops which are detailed in Py *et al.* (2005). The motion of two crop canopies of alfalfa and wheat is video-recorded from the edge of the field under various wind conditions, see Figure 2. A network of thin ranging poles, planted in the crop with a spacing of 1.5 m, is used as reference marker for subsequent image distortion correction. This differs from Py *et al.* (2005). During each sequence of video-recording, lasting 10 to 30 seconds, the wind velocity is simultaneously measured with a hot wire anemometer located just above the crop surface. This allows us to relate the patterns of the crop motion to the intensity of wind. The spatio-temporal motion of the upper crop surface is deduced from a sequence of images, after correcting for perspective distortion, by a correlation analysis: the computation is based on standard Particle Image Velocimetry (PIV) algorithms (Raffel *et al.* 1998), with the small scale heterogeneities of the plants playing the role of natural tracers. This measurement technique yields a

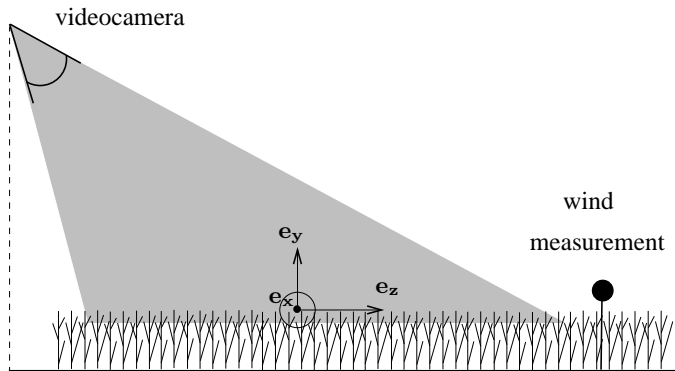


FIGURE 2. Experimental set-up for the measurement of the wind-induced motion of crops.

two-dimensional spatio-temporal horizontal velocity field $\mathbf{V}(x, z, t)$ of the canopy surface with high spatial and temporal resolution.

In order to extract the coherent structures of the canopy motion, we then use a Bi-Orthogonal Decomposition (BOD, see Aubry, Guyonnet & Lima (1991)) of the crop velocity field $\mathbf{V}(x, z, t)$. This Bi-Orthogonal Decomposition reads

$$\mathbf{V}(x, z, t) = \sum_{k=1}^N \sqrt{\alpha_k} \mu_k(t) \Psi_k(x, z), \quad (2.1)$$

where Ψ_k , referred to as *topos*, are the spatial modes and μ_k , referred to as *chronos*, are the temporal modes. See Hémon & Santi (2003) for a recent review on BOD, and Py *et al.* (2005) for the application of BOD in the context of crop motion. In practice, topos and chronos are, respectively, velocity maps and time functions. They form a set of normalised orthogonal functions, and the spatio-temporal modes (Ψ_k, μ_k) in (2.1) are ranked in descending order of their kinetic energy α_k . A typical set of BOD modes is shown in Figure 3 with the two most energetic topos and associated chronos derived from a sequence of motion of a wheat field under wind. The topos, Figure 3(a) and (b), display patterns of motion. A two-dimensional Fourier transform of Ψ_k ($k=1,2$) yields the characteristic wavenumbers k_x and k_z in the x - and z - directions. The corresponding

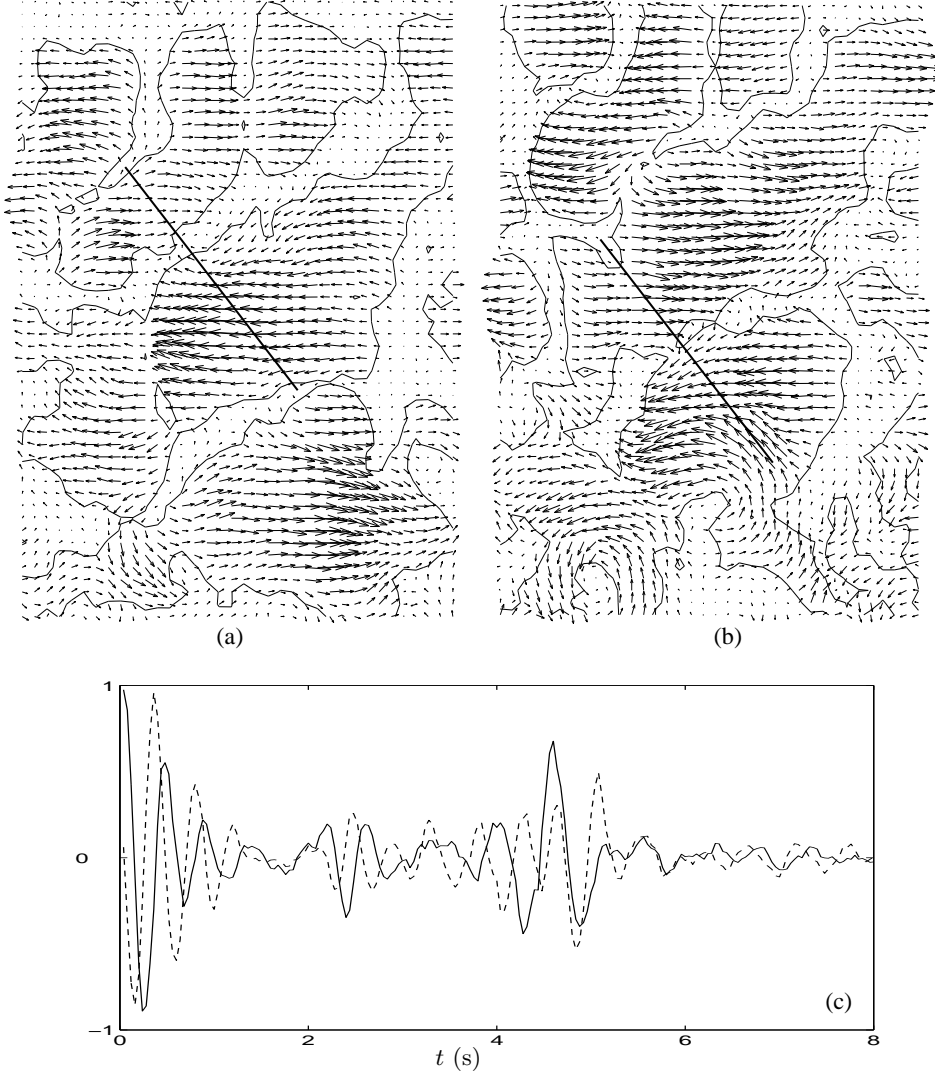


FIGURE 3. Velocity field and iso-contour of modulus of the two most energetic topois (a, b) and the associated chronos ((c), (—) chronos 1, (- -) chronos 2) derived from the BOD analysis of a sequence of motion of a wheat field under wind. The wavelenghts of the topois, derived from two-dimensional Fourier analysis, Eq. (2.2), and represented by the straight line, are $\lambda_1 = \lambda_2 = 1.4$ m, and the oscillation frequencies of the chronos are $f_1 = f_2 = 2.2$ Hz, leading to a phase velocity for the coherent structures of $c = 3.1 \text{ ms}^{-1}$ in the direction of the line.

wavelenghts of each topois

$$\lambda = 2\pi / \sqrt{k_x^2 + k_z^2}, \quad (2.2)$$

characterising the spatial structure of the topos, are then deduced, see Figure 3. The associated chronos, Figure 3(c), display a regular oscillatory behavior. The oscillation frequencies f are measured using a Fourier transform of μ_k ($k=1,2$). We notice that the two topos display similar wavelengths λ and seem phase-lagged in space, and that the two chronos have similar frequencies f and also seem phase-lagged in time, see Figure 3. Consequently, the combination of these two phase-lagged spatio-temporal modes leads to a pattern propagating in the direction of the main wavelength vector, i.e. $\theta = \text{atan}(k_z/k_x)$, with a phase velocity $c = \lambda f$. The BOD analysis of the velocity field of the plant surface thus allows us to extract the propagating pattern of the crop canopy from a complex signal

In addition to the measurements of crop motion, the mechanical properties of the individual plants, for both canopies, are also measured. The mechanical properties of the stems are derived from free oscillation tests as proposed by Flesch & Grant (1992) and Doaré, Moulia & de Langre (2004). A single plant is isolated and clamped at its foot, the stem is displaced from its equilibrium position, then released, and its in-plane motion is video-recorded. Based on the resulting sequence of images, the oscillation of the stem is measured by tracking its position along a horizontal line versus time, see Figure 4. The natural vibration frequency f_0 of the plant is then derived via a Fourier transform. The spacing l between neighboring stems in a canopy, their height h as well as the mass distribution along the stem are also measured (Figure 4).

Both the video-recording of the crop motion and the measurement of the mechanical plant properties had to be performed within a few days such that the maturity of the plants, and thus their stiffness, would not significantly vary.

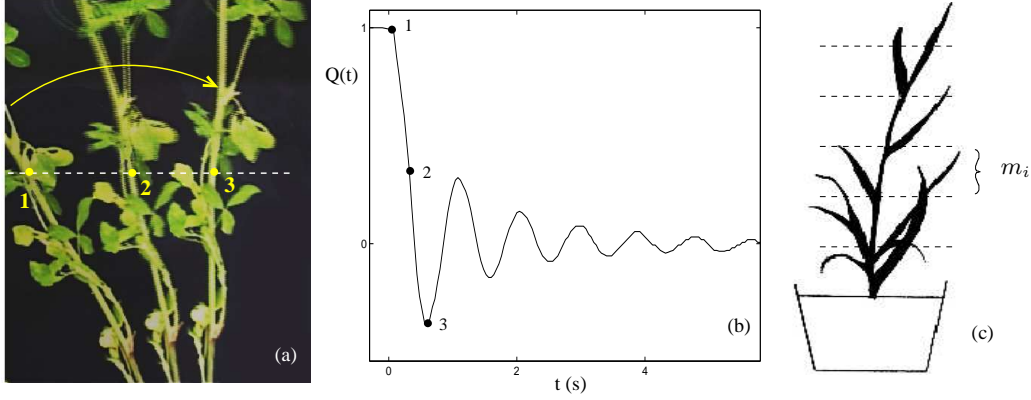


FIGURE 4. (a) Snapshot of the free oscillation test showing the instantaneous positions of a stem of alfalfa. (b) Oscillation of the stem as a function of time measured by tracking its position along a horizontal line. (c) Mass distribution measurement of a plant in 10 cm segments: m_i is the mass of the i^{th} segment.

2.2. Experimental results

The following experiments took place in May 2004 in Lusignan (France). The crops consisted of separate alfalfa (*Medicago sativa* L. cv Mercedes) and wheat (*Triticum aestivum* L. cv Apache) fields. The properties of six individual plants taken from the alfalfa field and four plants from the wheat field were measured, and the averaged results together with the corresponding range are given in Table 1. The two crop species were chosen for this study since they display different stiffness characteristics but similar height, at the growth stages at which they were sampled.

About thirty image sequences of the canopy motion under wind were recorded on both crops and analysed with the image correlation and BOD techniques described above. The values of the wavelength λ of the topos and frequency f of the chronos of the two most energetic modes were obtained for different values of the corresponding wind velocity U . Only the normalised results, λ/h and f/f_0 as a function of the reduced velocity U_r , are presented here, see Figure 5. The reduced velocity U_r , a classical non-

	f_0	h	m	l	r
	(Hz)	(m)	(10^{-3} kg)	(m)	(Nm $^{-1}$)
alfalfa	1.05	0.69	4.6	0.05	0.17
	[0.8-1.5]	[0.47-0.84]	[1.3-6.2]		
wheat	2.50	0.68	1.5	0.05	0.41
	[2.0-3.0]	[0.54-0.76]	[0.7-1.8]		

TABLE 1. Measured properties of the crops of wheat and alfalfa (mean value and data interval): f_0 is the eigen-frequency, h the canopy height, m the modal mass (see Eq. (3.1)), l the spacing between plants, and r the flexural stiffness deduced from f_0 and m (see Eq. (3.2)).

dimensional parameter in fluid-structure interactions, see for instance Blevins (1990), relates a characteristic velocity of the fluid, U , to a characteristic velocity of the solid, in our case based on the free vibration frequency f_0 and canopy height h . We obtain

$$U_r = \frac{U}{f_0 h}, \quad (2.3)$$

where f_0 and h are values measured for the individual plants of each canopy, Table 1. For both canopies, the normalised wavelength λ/h was found, to increase with the reduced velocity U_r , see Figure 5(a). For a given value of the dimensional wind velocity U , the dimensional wavelength λ was 2 to 3 times larger for alfalfa than for wheat. Therefore, since f_0 is the only parameter in the normalisation whose value significantly differs between wheat and alfalfa, the similarity of the data for both canopies regarding their dependance on U_r demonstrates that plant rigidity must be accounted for when determining the wavelength of the coherent crop motion.

The normalised frequency of the chronos f/f_0 was found to be approximately independent of the reduced velocity U_r for both canopies, see Figure 5(b). The mean value of f/f_0 was close to 1 for alfalfa (1.06) but seemed to be slightly lower than 1 for wheat

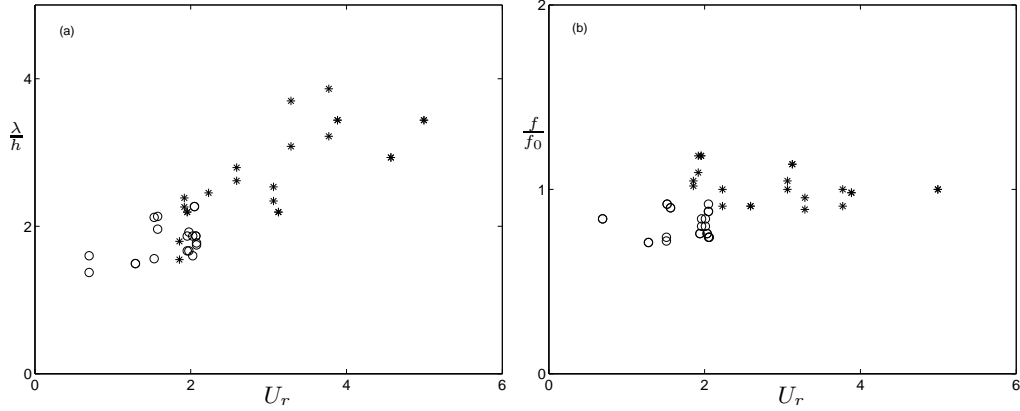


FIGURE 5. Wave properties of the first two modes of the BOD analysis of the measured canopy motion: characteristic wavelength of the topos normalised by the canopy height h (a), and frequency of the chronos normalised by the frequency of the plants f_0 (b) as a function of the reduced velocity U_r . (*) alfalfa field, (o) wheat field.

(0.81). However, Figure 5(b) does not take into account the variability of f_0 , see Table 1. A detailed statistical analysis accounting for both the variability on f and f_0 , based on the first analogue of Fieller's theorem, the use of Berhens distributions and the Sukhatme d-test (Finney 1964), showed that the confidence limits of f/f_0 were not significantly different between both canopies and that f/f_0 was close to 1 in both cases. The apparent lower value of f/f_0 for wheat in Figure 5(b) is likely to have resulted from an underestimation of f_0 in our plant sample due to the large spread of f_0 values due to the plants' biological variability. In conclusion, our experimental data demonstrate that the coherent motion of the crop under wind occurs near the natural vibration frequency of the plants, independent of the wind velocity.

2.3. Discussion

The experimental results shown above are the first quantitative and extensive measurement of the coherent waving of crop canopies under wind. The most energetic modes of the BOD revealed large scale coherent structures in space. Such a large correlation

length does not appear naturally in a set of adjacent oscillating stems and thus suggests the existence of an underlying instability mechanism. The identification of large coherent structures in the motion of the crops provides evidence that the shear-layer type instability, governing the wind dynamics over plant canopies (Raupach *et al.* 1996), also drives the motion of the canopy. Moreover, the measured wavelengths of the topos, scaled by the height of the plants ($1 < \lambda/h < 4$), are of the same order as the size of the coherent structures of wind measured over wheat and corn canopies, $3 < \lambda/h < 5$, see Raupach *et al.* (1996) and Finnigan (2000).

In shear layer instabilities, the wavelength is governed by the vorticity thickness of the mean flow profile (Huerre 2000). In the context of wind-driven plant canopies, the vorticity thickness δ (Figure 1), which is mainly linked to the leaf area density of the canopy, is known to be independent of the wind velocity U , see Brunet & Irvine (1999). Following the mixing layer analogy of Raupach *et al.* (1996), the wavelength would thus be expected to be independent of U . On the present study, however, the wavelength characterising the coherent wave patterns of the crop was experimentally shown to increase significantly with U while the associated frequency was independent of U , see Figure 5. This fact may not be explained by the mixing layer analogy of Raupach *et al.* (1996).

Moreover, the bending rigidity of the plants, via their natural frequency f_0 , was shown to play a dominant role in the scaling of wavelength and frequency, as extracted from the measured motion of the wheat and alfalfa crops. In particular it is striking that the coherent wave motion occurs at the free vibration frequency f_0 of the plants independently of the wind velocity. This frequency selection of the coherent motion of the crop suggests that the dynamics of the plants plays an active role in the underlying instability mechanism. Finnigan (1979) also found peaks in the velocity spectra of wind over waving wheat that matched the free vibration frequency of the wheat stems: this fact

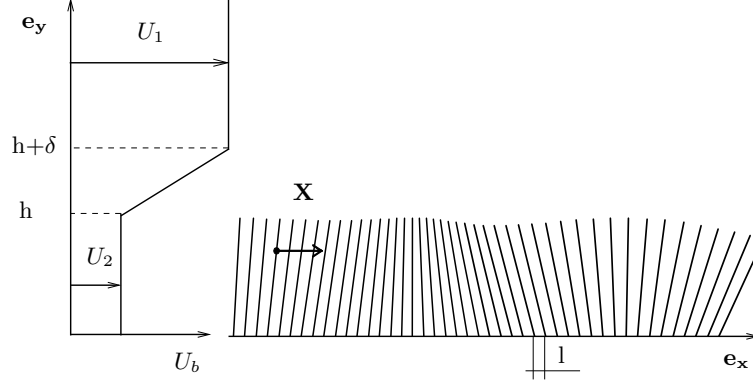
also suggests that the coherent oscillation of the plants may perturb the wind flow over and inside the canopy. The mixing layer model proposed by Raupach *et al.* (1996) does not provide an explanation for the role of the canopy dynamics as suggested by both our results and those of Finnigan (1979). To remedy this, a model that couples wind dynamics and canopy motion, is proposed and analysed in the following Section.

3. A model coupling mixing layer dynamics and crop motion

3.1. Description of the model

Here we investigate the effect of the plants' dynamics on the instability that simultaneously causes large scale vortical structures of the wind and coherent wave motion of the crop canopies. A coupled model is proposed in which both the wind flow over and inside the canopy and the motion of the plants are considered and where both media interplay. A preliminary version of this model was presented in Py, de Langre & Moulia (2004).

Crop plants are commonly modeled as mechanical oscillators, see for instance Flesch & Grant (1991); Farquhar *et al.* (2003); Doaré *et al.* (2004). The vibration tests performed on the wheat and alfalfa stems, see Section 2, confirmed that most of the dynamics of the plant may be represented by such a model. We describe the crop canopy as an infinite row of identical oscillators, see Figure 6. Elastic interactions may be introduced to model the contacts between neighboring plants (Doa re *et al.* 2004; Py *et al.* 2004), but these interactions were found to have only a small effect and are neglected for the sake of clarity. Following Do re *et al.* (2004), the crop canopy is modelled as an equivalent continuous medium, Figure 6, and its motion is described by the horizontal displacement $\mathbf{X}(x, y, t) = \chi(y) Q(x, t) \mathbf{e}_x$, where χ represents a mode shape and Q denotes the corresponding generalised displacement. In what follows, only the fundamental mode of vibration of the stems is considered, using a simplified linear mode shape $\chi = y/h$. The inertia of the

FIGURE 6. Basic flow U_b and model of the crop canopy.

plant is taken into account via the modal mass,

$$m = \int_0^h m_l(y) \chi^2 dy, \quad (3.1)$$

where m_l is the mass distribution measured in segments, see Figure 4(c). The modal stiffness of the stem is then defined as

$$r = (2\pi)^2 m f_0^2. \quad (3.2)$$

The damping of the mechanical oscillators will be neglected as dissipation is not expected to play a dominant role in the instability mechanism.

We assume that the canopy movement results from a local streamwise drag force acting on the equivalent surface of each plant and depending on the difference between the local horizontal wind velocity, \mathbf{U} , and the horizontal plant velocity, $\mathbf{V} = \partial \mathbf{X} / \partial t$. This drag force is then projected onto the mode shape χ (Blevins 1990). The dynamics of the canopy is thus governed by

$$m \frac{\partial^2 Q}{\partial t^2} + r Q = \int_0^h \frac{1}{2} \rho C_D [(\mathbf{U} - \mathbf{V}) \cdot \mathbf{e}_x]^2 \chi dy, \quad (3.3)$$

where C_D is a dimensional drag coefficient assumed to be uniform along the plant height. This coefficient may be estimated from the static deflection of the plant under wind load.

The wind velocity \mathbf{U} is governed by the Euler equations within and above the canopy;

again, the effect of fluid viscosity is neglected as the mixing layer instability mechanism, expected to play a major role in the wind dynamics (Raupach *et al.* 1996), is known to be essentially inviscid (Huerre & Rossi 1998). A source term representing the effect of the drag load on the fluid flow is added to the x -momentum equation inside the canopy ($y < h$).

In order to model the inflectional mean wind profile, see Figure 1, we use a piecewise linear profile $U_b(y)$, defined by a vorticity thickness δ and a shear parameter $R = (U_1 - U_2)/2U$ based on the mean velocity $U = (U_1 + U_2)/2$, see Figure 6. This type of profile is commonly used to model mixing layer configurations and, despite its simplicity, has been shown to capture the main characteristics of the instability (Huerre & Rossi 1998).

To investigate the stability of a given basic state, composed of a basic velocity profile U_b and pressure P_b , together with the corresponding equilibrium position of the canopy Q_b , we introduce the associated small perturbations u, v, p, q . The momentum and mass balance for the flow and the dynamic equation for the canopy may then be expanded to first order in terms of the perturbations, which yields the set of coupled equations:

$$\frac{\partial u}{\partial t} + U_b \frac{\partial u}{\partial x} + \frac{\partial U_b}{\partial y} v = -\frac{1}{\rho} \frac{\partial p}{\partial x} - \frac{C_D}{l^2} U_2 \left(u - \chi \frac{\partial q}{\partial t} \right) \quad (3.4)$$

$$\frac{\partial v}{\partial t} + U_b \frac{\partial v}{\partial x} = -\frac{1}{\rho} \frac{\partial p}{\partial y} \quad (3.5)$$

$$\nabla \cdot \underline{u} = 0 \quad (3.6)$$

$$m \frac{\partial^2 q}{\partial t^2} + r q = \int_0^h \rho C_D U_2 \left(u - \chi \frac{\partial q}{\partial t} \right) \chi dy, \quad (3.7)$$

where the drag coefficient C_D in (3.4) is set to zero outside the canopy ($y > h$). Using the vorticity thickness δ , the advection time δ/U and the mass $\rho\delta^3$, we may define the nondimensionalized variables:

$$\bar{m} = \frac{m}{\rho\delta^3}, \quad \bar{r} = \frac{r}{\rho\delta U^2}, \quad \bar{h} = \frac{h}{\delta}, \quad \bar{l} = \frac{l}{\delta}, \quad \bar{C}_D = \frac{C_D}{\delta},$$

$$\bar{u} = \frac{u}{U}, \quad \bar{v} = \frac{v}{U}, \quad \bar{p} = \frac{p}{\rho U^2}, \quad \bar{q} = \frac{q}{\delta}, \quad \bar{x} = \frac{x}{\delta}, \quad \bar{t} = \frac{tU}{\delta}.$$

A traveling wave solution is then sought in the form: $(\bar{u}, \bar{v}, \bar{p}, \bar{q}) = \text{Re}[(\hat{u}, \hat{v}, \hat{p}, \hat{q}) e^{i(\bar{k}\bar{x} - \bar{\omega}\bar{t})}]$.

Assuming irrotational flow (Drazin & Reid 1981), the corresponding dispersion relation is eventually obtained as

$$D(\bar{k}, \bar{\omega}) = (D_{solid} + A)(D_{fluid} + E) + G = 0, \quad (3.8)$$

where the terms on the right hand side are given in Appendix A. In the above expression D_{fluid} and D_{solid} are, respectively, the dispersion relations of the fluid flow and canopy motion without coupling, and A, E and G are coupling terms involving the drag coupling coefficient \bar{C} . For the sake of clarity the overbars on \bar{k} and $\bar{\omega}$ will be omitted from now on.

For the analysis of the model, we use the mechanical and geometrical properties measured on the alfalfa crop, see Table 1, a mean flow velocity of $U = 3 \text{ ms}^{-1}$ and flow profile characteristics given in Raupach *et al.* (1996) for this type of canopies, namely, $R = 0.5$ and $\delta = Rh$. For the drag coefficient, we use $C_D = 10^{-2}$ m ($\bar{C} = 2.9 \cdot 10^{-2}$), corresponding to a static deflection of the plants of 10 cm at their top for a wind velocity of $U = 3 \text{ ms}^{-1}$. These parameter values are used in the following analysis, except when specified otherwise.

3.2. Temporal stability analysis of the coupled model

The temporal stability of propagating waves in the wind and of the canopy motion is analysed by numerically calculating the complex frequency ω associated with a specified real wavenumber k by solving the dispersion relation (3.8) with the parameter values given above. Four temporal branches $\omega(k)$ result from the dispersion relation (3.8) with $\omega_i = \text{Im}(\omega)$ as the instability growth rate and $\omega_r = \text{Re}(\omega)$ as the temporal frequency. As k is varied a pocket of instability with $\omega_i > 0$ is found. Only the branch with the most amplified growth rate is considered, and illustrated in Figure 7.

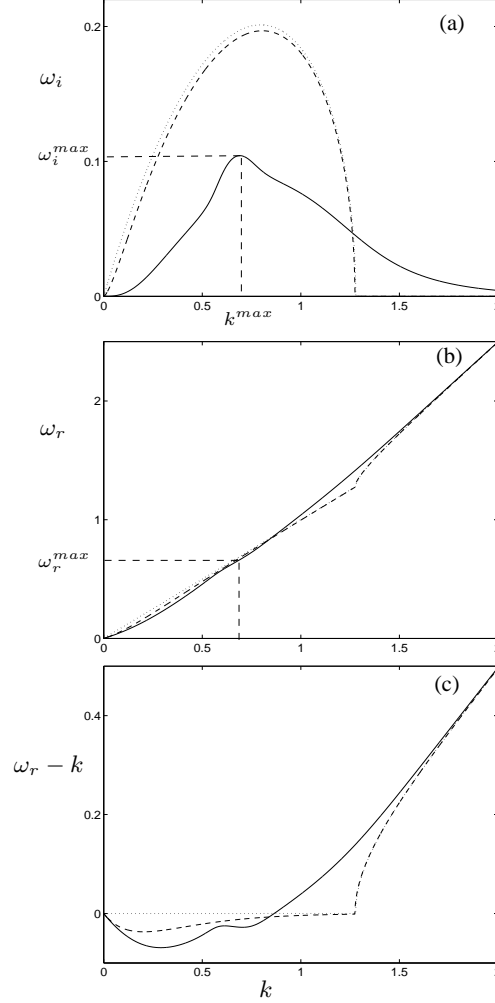


FIGURE 7. Most unstable temporal branch derived from the model: growth rate ω_i , frequency ω_r and effective frequency $\omega_r - k$ (same as ω_r without the advection) versus wavenumber k . (—) coupled model, (- -) $C = 0$: Kelvin-Helmholtz in a bounded domain, ($\cdot \cdot \cdot$) $C = 0$ and $\bar{h} \rightarrow \infty$: Kelvin-Helmholtz in an infinite domain (Huerre & Rossi 1998).

We first investigate the origin of the instability of the coupled system by varying the drag coupling coefficient \bar{C} and the canopy height \bar{h} , Figure 7. When decreasing \bar{C} , the most unstable $\omega_i(k)$ branch deforms and, for $\bar{C} = 0$, coincides with the unstable branch of the Kelvin-Helmholtz instability in a bounded domain, i.e. the solution of $D_{fluid}(k, \omega) = 0$, see Figure 7(a). Then, as the non-dimensional canopy height $\bar{h} = h/\delta$

tends to infinity, the temporal Kelvin-Helmholtz branch for a piecewise linear profile in an infinite medium is recovered, with the most amplified wavenumber at $k^{max} = 0.8$ (Huerre & Rossi 1998). We may thus state that the unstable branch of the coupled model stems from the unstable Kelvin-Helmholtz branch. This shows that the mixing layer instability remains the main instability mechanism over plant canopies when wind and canopy dynamics are coupled.

In addition, the mode shapes of the flow perturbation associated with the most unstable wave ($k = k^{max}$, $\omega = \omega_r^{max} + i\omega_i^{max}$) of (3.8) are displayed in Figure 8 for the coupled and uncoupled cases: the velocity field $\{u, v\}(x, y)$ is slightly modified by the coupling but inherits the characteristics of the Kelvin-Helmholtz instability.

The fact that the coupled wind-canopy instability is driven by a mixing layer type instability is in agreement with experimental results and the theory proposed by Raupach *et al.* (1996). The wavelength of the instability is thus principally governed by the vorticity thickness δ of the mean wind profile, as found experimentally by Raupach *et al.* (1996). However, as the most unstable branch is deformed when the coupling coefficient \bar{C} is varied, see Figure 7, the properties of this instability are modified by taking into account the motion of the canopy. Wind and wind-induced motion of the canopy are thus governed by a modified Kelvin-Helmholtz instability.

Coupling by a drag force decreases the growth rate $\omega_i(k)$ of the instability and, in particular, the maximum growth rate ω_i^{max} , see Figure 7(a): dissipative effects in mixing layers are indeed known to be stabilizing, see for instance Panton (1996). The coupling also decreases the most amplified wavenumber k^{max} , in our case by about 15%, Figure 7(a). The decrease of k^{max} due to the coupling is associated with a decrease in the temporal frequency $\omega_r^{max} = \omega_r(k^{max})$ of the unstable wave, see Figure 7(b). It is therefore important to notice that the characteristic frequency resulting from the coupled insta-

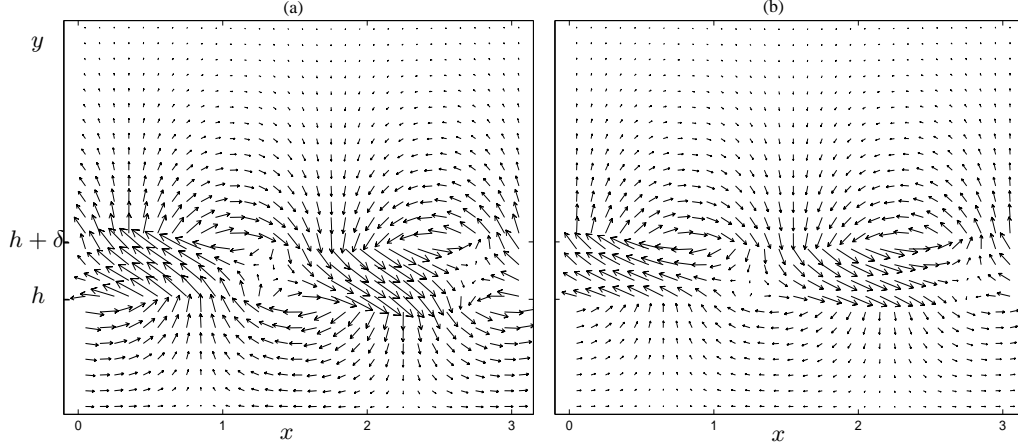


FIGURE 8. Velocity map of the flow perturbation (u, v) associated with the most unstable wave: (a) uncoupled model $C = 0$, (b) coupled model $C = 1$; normalised assuming $\hat{u}(h) = 1$ in both cases.

bility is smaller than the frequency that would be predicted if only the stability of the flow profile were taken into consideration. Moreover, the peak in the temporal growth rate in Figure 7(a) is narrower in terms of wavenumbers for the coupled model than it is for the uncoupled case. As a consequence, the instability is more selective in terms of wavenumbers when fluid and solid dynamics are coupled.

As was done for the most unstable branch, the origin of the three other branches of the coupled model may be understood by decreasing the drag coefficient \bar{C} . When $C = 0$, the dispersion relation (3.8) is reduced to $D_{fluid} D_{solid} = 0$, and in this limit it can be shown that two branches correspond to the Kelvin-Helmholtz solution in a bounded domain and the two remaining branches correspond to the solution of the canopy equation, $\omega = \pm\sqrt{r/m}$. Each of the four temporal branches is then deformed when coupling is taken into account.

The stability analysis of the coupled fluid-structure model has shown that wind and wind-induced motion of the canopy are governed by a modified shear layer instability.

Taking into account the dynamics of the plants through a drag term does modify the instability characteristics.

3.3. Effect of the frequency of the canopy: a lock-in mechanism

In this section we study the influence of the canopy parameters on the properties of the coupled instability. Keeping all other parameters constant, we vary the non-dimensional flexural stiffness \bar{r} of the plants. Varying \bar{r} modifies the four temporal branches of the dispersion relation (3.8) and, in particular, it affects the shape of the most unstable $\omega_i(k)$ branch shown Figure 7. We may therefore follow the paths of the most amplified wavenumber k^{max} and of the corresponding growth rate ω_i^{max} and frequency ω_r^{max} as the stiffness of the canopy is varied. The evolution of ω_i^{max} and ω_r^{max} as a function of the dimensionless frequency of the canopy

$$\bar{f}_0 = \sqrt{\frac{\bar{r}}{\bar{m}}} = \frac{2\pi\delta}{h} \frac{1}{U_r} \quad (3.9)$$

is shown Figure 9. For completeness we also show the reference values corresponding to the uncoupled model of the pure mixing layer instability with $\bar{C} = 0$. Note that the evolution of k^{max} as a function of \bar{f}_0 (not shown) is equivalent to that of ω_r^{max} since k^{max} and ω_r^{max} are quasi-proportional to each other (exactly proportional in the pure Kelvin-Helmholtz instability), see Figure 7(b).

While the frequency ω_r^{max} , Figure 9(b), is found to be nearly constant for small and large values of \bar{f}_0 , there exists a range, in our case from $\bar{f}_0 = 0.36$ to 1.24, where it varies almost linearly with \bar{f}_0 , thus deviating from its asymptotic values. We may state that in this range the frequency of the instability *locks* onto the frequency of the plants as its value approaches and follows that of the plants. This is identical in form, but distinct in mechanism, to what is observed in vortex-induced vibrations (Williamson & Govardhan 2004), and the term lock-in shall be used from now on. In this same lock-in

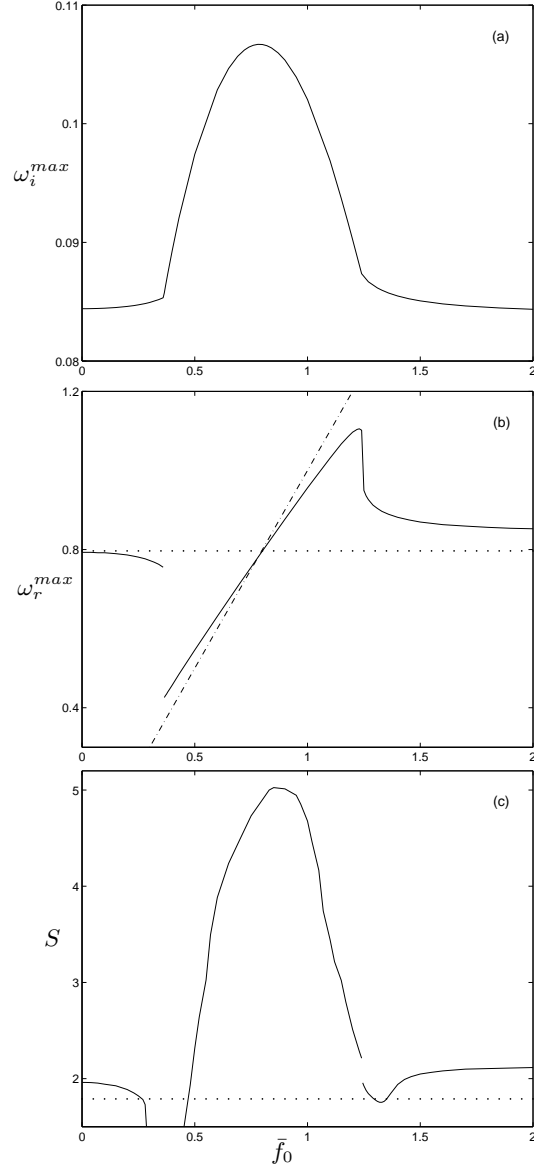


FIGURE 9. Evolution of the growth rate ω_i^{max} , frequency ω_r^{max} and selectivity S of the coupled instability with the natural vibration frequency of the plants \bar{f}_0 showing a lock-in mechanism. (—) present coupled model, ($\cdot\cdot\cdot$) uncoupled model ($\bar{C} = 0$), ($-\cdot-$) perfect frequency lock-in where the instability frequency would be that of the plants ($\omega_r^{max} \equiv \bar{f}_0$).

range the growth rate of the instability, ω_i^{max} , Figure 9(a), also strongly deviates from its asymptotic regime and reaches a maximum near $\bar{f}_0 = 0.8$.

The evolutions of ω_r^{max} and ω_i^{max} described above result from the deformation of

the most unstable branch of the dispersion relation (3.8) as we vary the parameters. In particular, the jumps of ω_r^{max} shown Figure 9(b) occur as the most unstable $\omega_i(k)$ branch displays two almost equally amplified bumps: varying \bar{f}_0 , one bump, initially less amplified, becomes suddenly more amplified than the other, leading to a jump in k^{max} and, consequently, in ω_r^{max} . This also explains why the abrupt variations of the frequency are associated with a smooth variation of the growth rate.

The selectivity of the instability in terms of wavenumbers is also affected by the variation of the canopy frequency \bar{f}_0 , as illustrated Figure 9(c). The selectivity, noted S , is defined as the inverse of the passing band of wavenumbers for which the growth rate is above a certain threshold, say $\omega_i/\omega_i^{max} > 0.9$, measured in terms of normalised wavenumbers k/k^{max} . Figure 9(c) reveals that the selectivity of the instability is significantly increased in the lock-in interval when compared to the asymptotic values or to those of the uncoupled model ($\bar{C} = 0$). Moreover, the frequency \bar{f}_0 for which S is maximum, i.e for which the coupled instability is the most selective, is approximately equal to the frequency of the canopy leading to the maximum amplification of the growth rate ($\bar{f}_0 = 0.8$), see Figures 9(a) and (c). The variation of the instability selectivity and the lock-in mechanism are therefore linked. In other words, the modification of the shear layer instability by the frequency lock-in leads to a more selective coupled instability.

3.4. Robustness of the lock-in mechanism

The influence of the canopy stiffness on the characteristic frequency, growth rate and selectivity of the coupled instability was shown above using a fixed set of parameters for the model, namely, the properties of alfalfa plants given in Table 1 and a drag coefficient $\bar{C} = 2.9 \cdot 10^{-2}$. Yet, depending on the maturity of the plants for instance, their mass and geometry may vary. This variation is even more dramatic when comparing plants from different species: see for instance the difference in mass between alfalfa and wheat

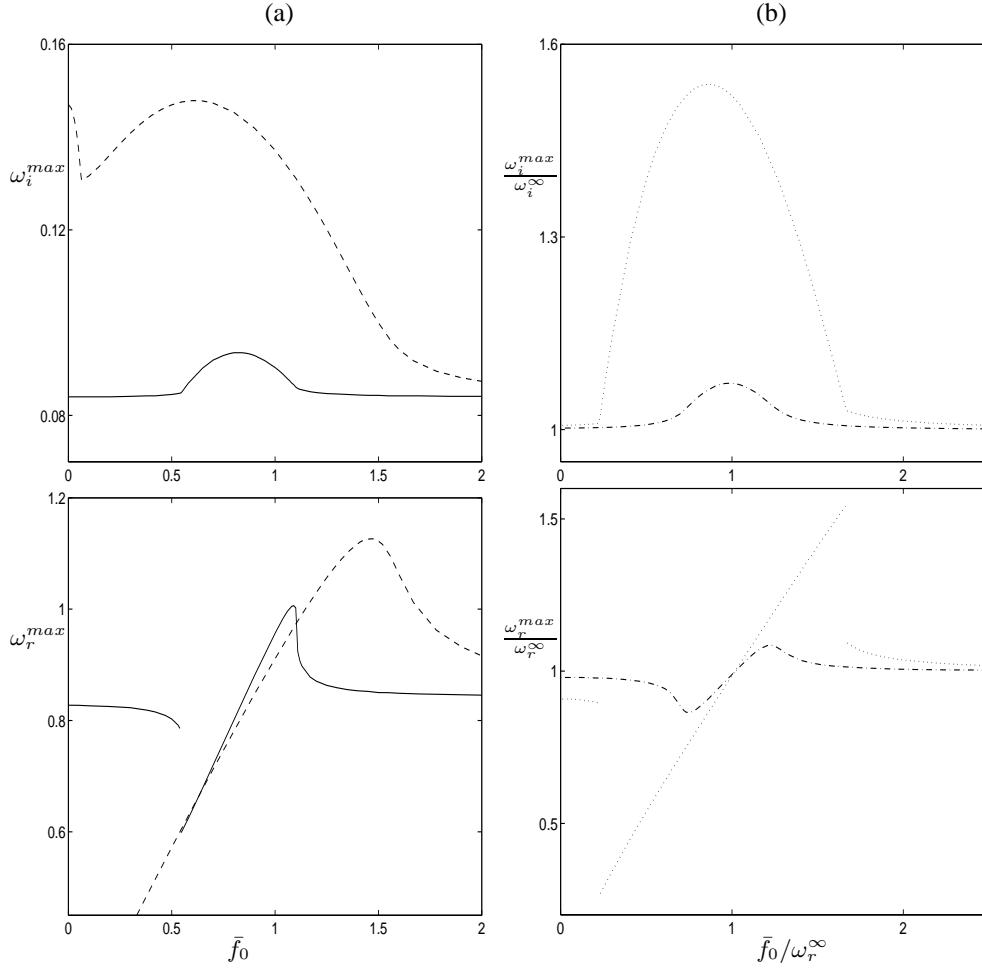


FIGURE 10. Effect of the canopy mass and of the drag coupling coefficient on the evolutions of ω_i^{max} and ω_r^{max} versus \bar{f}_0 . (a) (—) high mass $\bar{m} = 0.25$, (- -) low mass $\bar{m} = 0.01$. (b) (- -) high drag $\bar{C} = 4.3 \cdot 10^{-2}$, ($\cdot \cdot \cdot$) low drag $\bar{C} = 1.4 \cdot 10^{-2}$.

(Table 1). In order to check whether the frequency lock-in shown above is an effect specific to the alfalfa crop, or a more general mechanism, we now explore the effect of the parameters of the model. Two major effects are illustrated Figure 10: that of the inertia of the canopy given by the non-dimensional mass \bar{m} , and that of the level of coupling between the wind dynamics and the motion of the canopy given by the drag coupling coefficient \bar{C} .

As far as the mass is concerned, the influence of \bar{f}_0 is shown for a heavy and a light

canopy by considering a mass three times higher than that of alfalfa and a mass two times smaller than that of wheat, Figure 10(a). In both cases, a similar behavior as before is found for the evolutions of ω_r^{max} and ω_i^{max} : for intermediate values of the frequency of the canopy \bar{f}_0 , the instability frequency locks onto \bar{f}_0 , with marked increase in the growth rate. The frequency lock-in is more pronounced when the mass of the plants is high, but persists over a larger interval of \bar{f}_0 when the canopy is light. The corresponding increase in the growth rate in the lock-in interval is weaker for the heavy canopy.

Considering a fixed mass of the canopy, we now study the effect of varying the drag coupling coefficient \bar{C} . In the previous section, $\bar{C} = 2.9 \cdot 10^{-2}$ was considered; one higher and lower value is now taken into account, namely, $\bar{C} = 1.4 \cdot 10^{-2}$ and $\bar{C} = 4.3 \cdot 10^{-2}$. The evolutions shown Figure 10(b) for both cases are normalised by the asymptotic values of the growth rate and frequency, denoted ω_i^∞ and ω_r^∞ , obtained as $\bar{f}_0 \rightarrow \infty$ for the chosen value of \bar{C} . In this way, only the effect of \bar{C} on the lock-in mechanism is investigated. First, Figure 10(b) shows that the lock-in mechanism described previously at $\bar{C} = 2.9 \cdot 10^{-2}$ persists at smaller and larger drag coefficients. The lock-in range as well as the rate of change of ω_r^{max} with \bar{f}_0 both increase with the coupling coefficient \bar{C} . Moreover, the associated increase in the growth rate is stronger as the coupling \bar{C} increases. All this suggests that the stronger the fluid and solid dynamics are coupled, the more the canopy oscillation is able to perturb, via the lock-in mechanism, the Kelvin-Helmholtz instability resulting from the inflectional wind profile. In the four cases shown Figure 10, the variations of the frequency and growth rate of the instability are associated with an increase of the selectivity S in the lock-in interval (not shown). The increase of the selectivity of the coupled instability linked to the lock-in mechanism, as shown Figure 9(c), therefore persists at different mass and drag coupling coefficients.

We have shown that taking into account the motion of the canopy via the drag load

affects the coupled instability. Not only does the canopy dynamics modify the properties of the Kelvin-Helmholtz waves, it also dominates the instability mechanism over a range of parameters. When the frequency of the canopy is close to the natural frequency of the instability, the latter deviates from the expected value and locks onto the free oscillation frequency of the plants, thus inducing an intensification of the instability and an increase of its selectivity. This mechanism is robust as it was shown to persist for plants of different mass and over a wide range of drag coupling coefficients.

3.5. Elementary lock-in model

In an attempt to clarify the lock-in mechanism by which the vibration frequency of the canopy dominates the instability frequency, we propose a simplified coupled model. In the complete model, Section 3, the canopy is treated as a continuum of mechanical oscillators and is linked to the wind flow by a dissipative drag coupling. This model was shown to be governed by a modified Kelvin-Helmholtz instability. In a reference frame moving at the mean advection velocity U , the Kelvin-Helmholtz waves correspond to a temporal oscillation whose amplitude increases exponentially with time. The temporal flow dynamics may thus be schematically represented by an unstable fluid oscillator, denoted $\varphi(t)$, with a characteristic mass, eigen-frequency and amplification rate, as in other analyses of lock-in, such as in the field of vortex-induced vibrations (Facchinetti *et al.* 2004; de Langre 2005). This fluid oscillator and the solid oscillator, $q(t)$, which represents the canopy, are then coupled by a dissipative force, corresponding to the linearized drag load in (3.4) and (3.7), and dependent on the difference between their respective velocities. After normalisation by the mass and frequency of the fluid oscillator,

the simplified model is thus governed by the following set of coupled linearised equations:

$$\frac{\partial^2 \varphi}{\partial t^2} - \xi \frac{\partial \varphi}{\partial t} + \varphi = \alpha \left(\frac{\partial q}{\partial t} - \frac{\partial \varphi}{\partial t} \right) \quad (3.10)$$

$$\mu \left(\frac{\partial^2 q}{\partial t^2} + \Omega^2 q \right) = -\alpha \left(\frac{\partial q}{\partial t} - \frac{\partial \varphi}{\partial t} \right), \quad (3.11)$$

where ξ is the instability growth rate of the fluid oscillator, μ and Ω are the non-dimensional mass and eigen-frequency of the solid respectively, and α is a coupling coefficient.

Considering $(\varphi, q) = \text{Re} [(\hat{\varphi}, \hat{q})e^{-i\omega t}]$, the frequency equation is easily obtained as:

$$\mathcal{D}(\omega) = (-\omega^2 - i(\alpha - \xi)\omega + 1) \left(-\omega^2 - i\frac{\alpha}{\mu}\omega + \Omega^2 \right) + \frac{\alpha^2}{\mu}\omega^2 = 0. \quad (3.12)$$

A typical plot of the most unstable solution $(\omega_i^{max}, \omega_r^{max})$ derived from (3.12) as a function of the frequency Ω of the solid oscillator is shown Figure 11 for an arbitrary set of parameters. The essential characteristics of the frequency lock-in obtained for the complete wind-canopy model are captured by this elementary model: within a certain range of solid frequencies Ω , the most unstable frequency ω_r^{max} deviates from its asymptotic regime and increases linearly with Ω , Figure 11(b), while simultaneously the growth rate ω_i^{max} increases substantially, see Figure 11(a). The maximum of the growth rate, obtained at the center of the lock-in interval of Ω , is always reached for $\Omega = 1$, which means that the most intense coupled instability occurs when the solid and fluid frequencies coincide. Outside the lock-in interval, for Ω small or large with respect to 1, the most unstable solution tends toward the solution of Eq. (3.10) when $\partial q/\partial t$ is neglected: in other words, the instability in this regime is governed by the fluid mode modified by the coupling coefficient α .

The frequency lock-in persists as the parameters of the elementary model are varied. The width of the lock-in range increases with the coupling coefficient α and decreases with the mass μ of the solid. The rate of change of ω_r^{max} with Ω as well as the relative

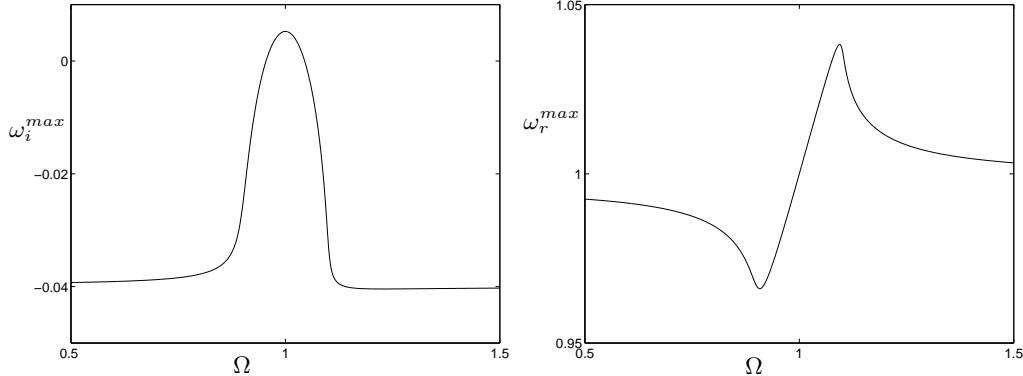


FIGURE 11. Most amplified growth rate and corresponding frequency derived from the elementary lock-in model as a function of the solid frequency Ω ($\alpha = 0.1$, $\xi = 0.02$, and $\mu = 1$). amplification of ω_i^{max} both increase with α and μ . These results are qualitatively in agreement with what was found for the complete wind-canopy model, where Ω in the simple model played the role of \bar{f}_0 .

This elementary model in which two oscillators, one unstable and one neutral, are coupled together, recovers the main features of the frequency lock-in mechanism governing the wind-canopy interaction of our general model. We may therefore state that the modification of the shear layer type instability, when taking into account the canopy motion, mainly results from a coupling between two frequencies: the natural frequency of vibration of the canopy and the frequency of the Kelvin-Helmholtz unstable waves related to the inflectional base flow. Note that although the mechanism of lock-in is often attributed to non-linear phenomena, as in Facchinetti *et al.* (2004), see also Williamson & Govardhan (2004), it corresponds in our case to a linear mechanism which may more simply be described by coupling two oscillators, as in de Langre (2005).

4. Comparison between the model and experimental results

The predictions of the coupled wind-canopy model are now compared to the experimental results on the coherent wave motion of crops under wind derived in Section 2. In

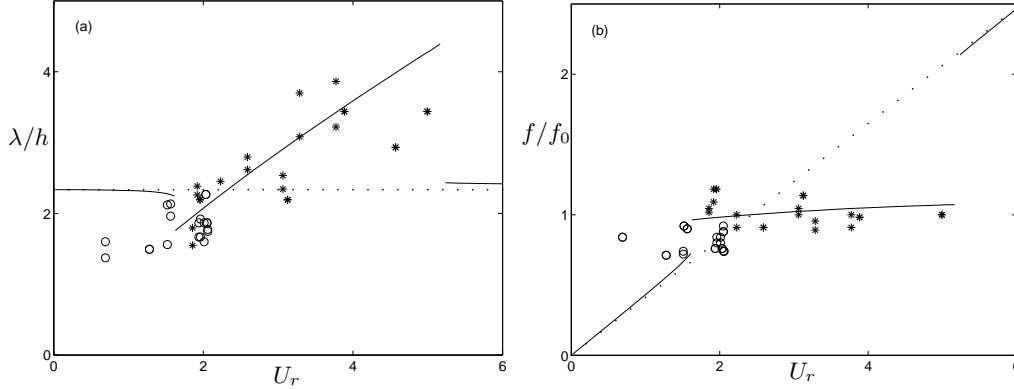


FIGURE 12. Comparison of the experimental results on the motion of alfalfa (*) and wheat (o) (reproduced from Figure 5) with the predictions of the coupled model (—): normalised wavelength (a) and frequency (b) versus reduced velocity. The dotted line (· · ·) represents the graphs resulting from the uncoupled mixing layer instability model, following Raupach *et al.* (1996).

Figure 12 the values of wavelength and frequency characterising the coupled instability of the model are compared to the corresponding experimental values derived from the BOD analysis of the motion of the wheat and alfalfa crops. For the model, the characteristic wavelength is derived from the most unstable wavenumber k^{max} , and the frequency from ω_r^{max} , both computed from the dispersion relation (3.8) using the experimental parameter values of alfalfa given Table 1 and varying the reduced wind velocity $U_r = U/f_0h$. For the sake of clarity only, we use the plant characteristics of alfalfa in the model for both crops.

Figure 12 shows good qualitative and quantitative agreement between the experimental and theoretical dependence of λ/h and f/f_0 on U_r . Moreover, the experimental points are mainly located in an interval of the reduced velocity U_r where the model predicts a lock-in of the instability frequency onto the free vibration frequency f_0 of the plants. It is thus the lock-in mechanism suggested by the analysis of the coupled model that explains why the coherent wave motion of the crops occurs at their eigen-frequency

independently of U as revealed by the experiments. The vortical structures of wind and the coherent motion of the plants are indeed due to a shear layer type instability linked to an inflectional wind profile. This Kelvin-Helmholtz mechanism would predict a wavelength set by the vorticity thickness of the profile, and thus independent of U , and furthermore a temporal frequency that increases with U (see the curves of the uncoupled model Figure 12). However, within the range of wind velocities from the experiments, the natural Kelvin-Helmholtz frequency is close to the free vibration frequency f_0 of the plants and, therefore, the instability frequency locks onto f_0 via the mechanism described in Sections 3.3 and 3.5. As a consequence, the frequency, see Figure 12(b), and the wavelength, see Figure 12(a), characterising the wind and canopy motion are, respectively, constant and increasing with U ; both are dependent on the canopy rigidity.

5. Discussion and concluding remarks

5.1. On the consequences of lock-in

The frequency lock-in of the shear layer type instability onto the natural frequency of the canopy provides new insight into some features of the wind dynamics over waving wheat (Finnigan 1979) and into characteristics of the coherent wave motion of crops under wind. These new findings remained unexplained by the mixing layer analogy of Raupach *et al.* (1996). The lock-in also confirms and clarifies the role of plant oscillations on the instability mechanism as suggested by Finnigan (2004).

Moreover, we showed in Section 3.3 that the lock-in mechanism increases the growth rate of the instability as well as its selectivity. When locked onto the oscillation frequency of the plants, the coupled instability is thus stronger and more efficient to select a specific wavelength and frequency from the turbulent disturbance environment. This intensification of the modified mixing layer instability by the frequency lock-in might

explain how this instability is able to develop over plant canopies in the presence of natural noise. Indeed the central frequency of the Kelvin-Helmholtz instability is known to be very sensitive to external noise (Huerre 2000): even in controlled laboratory experiments, the observation of the Kelvin-Helmholtz roll-up requires a forcing of the flow at the Kelvin-Helmholtz frequency. Questions thus arose on the way the shear layer instability can develop and persist in the wind over crops (Finnigan 2004). The role played by the oscillation of the plants, via the frequency lock-in mechanism, and its influence on the growth rate and selectivity of the instability make a valid contribution to explaining the occurrence of shear layer type instabilities on plant canopies.

5.2. *On the behavior outside the lock-in range*

Our experimental data fall within the range of the reduced velocities where lock-in occurs (Figure 12). Yet, if the plant canopy is very stiff or very compliant, or, equivalently, if the wind velocity is very low or very high, in other words for extreme values of the normalised canopy frequency \bar{f}_0 or the corresponding reduced velocity U_r , the coupled instability falls outside the interval required for lock-in. We may explore, in particular, the behavior of the coupled instability when the dynamics of the canopy is inhibited by very high plant stiffness ($\bar{r} \rightarrow \infty$). In this case, the dispersion relation (3.8) reduces to

$$D_{fluid} + E = 0. \quad (5.1)$$

The instability properties derived from the analysis of (5.1) are not identical to those of the uncoupled instability, i.e. the Kelvin-Helmholtz instability solution of $D_{fluid} = 0$. To understand the nature of the coupled instability in this limit, an asymptotic analysis of the stiff dispersion relation (5.1) is needed, where we assume the effect of the coupling term E to be small. This asymptotic analysis is detailed in Appendix B.

The most amplified frequency and growth rate derived from the asymptotic analysis,

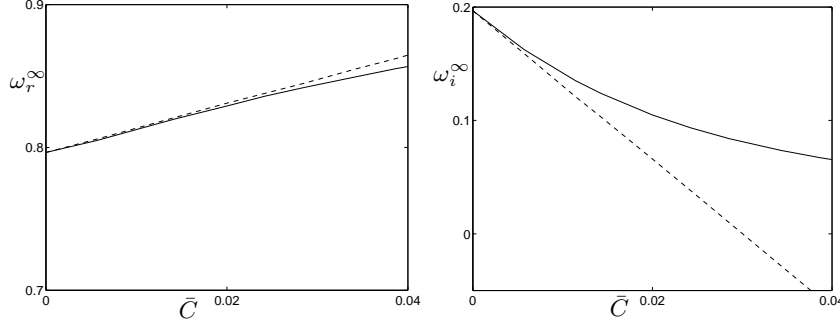


FIGURE 13. Frequency and growth rate of the limit model (5.1) versus drag coupling coefficient \bar{C} : comparison between the asymptotic approach (- -) and the exact solution (—). The evolution of the wavenumber is equivalent to that of the frequency.

Eq. (B 9), as a function of the drag coupling coefficient \bar{C} are compared to the exact solution of (5.1) in Figure 13. The asymptotic analysis provides a good estimation of the frequency ω_r^∞ and growth rate ω_i^∞ up to $\bar{C} \approx 0.03$. The accuracy of the asymptotic approach shows that the instability in the limit of $\bar{r} \rightarrow \infty$ is principally governed by the Kelvin-Helmholtz mechanism (D_{fluid}) but modified by the coupling term E.

The major effect of the coupling is to decrease the instability growth rate (Figure 13). The coupling also yields a small increase in the frequency (and wavenumber) of the instability. The reason for this is rather complex: the frequency is expected to decrease with dissipation rather than increase as is the case here. If we consider the stiff model (5.1) in the limit of $\bar{h} \rightarrow \infty$, which weakens the impact of the impermeability boundary condition on the ground, the coupling has non longer an effect on the instability frequency: ω_r^∞ is found to be constant with \bar{C} , whereas ω_i^∞ still decreases with \bar{C} , although at higher values. The modification of the Kelvin-Helmholtz frequency by the coupling for the case of a stiff canopy is thus related to the finite height of the canopy. We note that D_{fluid} itself is also affected by the canopy height (see the decrease of ω_i^{max} from $\bar{h} \rightarrow \infty$ to a finite \bar{h} in Figure 7(a)), the most amplified frequency of D_{fluid} , however, is not modified by \bar{h} .

To conclude, the instability for the case of a stiff canopy may be seen as a shear layer instability in a bounded domain modified by a dissipative term. Taking into account the presence of a stiff canopy induces a damping of the growth rate and a positive shift of both the frequency and the wavenumber of the instability related to the finite height of the canopy. These coupling effects are also present to various degrees in the general model for a flexible canopy, but are small compared to the variations induced by the lock-in.

Note that the behavior of the instability obtained for the limit $\bar{f}_0 \rightarrow 0$ or $U_r \rightarrow \infty$ is less realistic since in this limit the assumption of small canopy deflection becomes questionable.

5.3. On possible extensions of the model

The model considered in this study is linear and, consequently, finite amplitudes of the unstable modes cannot be reached. In the experiments presented here the amplitudes of the motion of the crop under wind could be measured. For each recorded sequence the amplitude is expressed as a space-averaged velocity W , defined by

$$W^2 = \frac{1}{N_s} \sum_{j=1}^{N_s} \sigma^2(M_j), \quad (5.2)$$

where $\sigma(M_j)$ is the standard deviation of $\mathbf{V}(t)$ at a point $M_j(x, z)$, and N_s is the number of spatial nodes. The results are presented in Figure 14(a) as a function the mean wind velocity U for both canopies. To normalise the data we use the growth rate ω_i^{max} of the coupled instability, resulting from the respective parameter values for wheat and alfalfa and the given value of U . The growth rate derived from the linear model is expected to show some influence on the amplitude, whatever the limiting mechanism may be. The normalised data, $W/\omega_i^{max}h$ as a function of the reduced velocity U_r , depicted in Figure 14(b), show a reasonably good agreement between the data of both canopies,

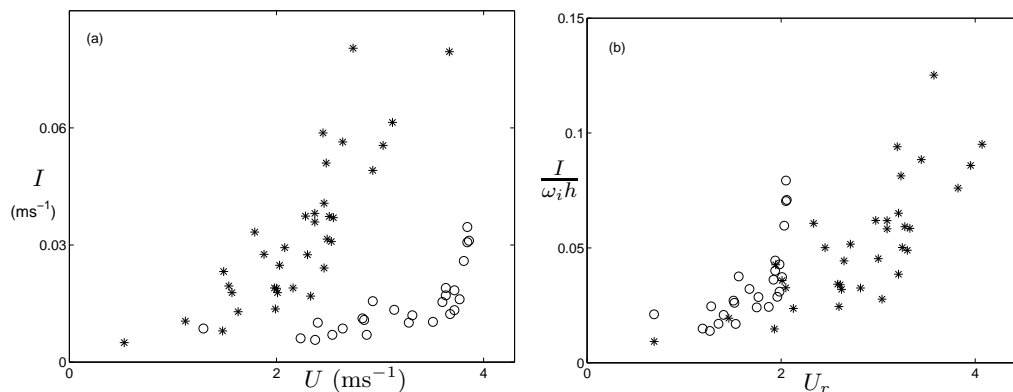


FIGURE 14. Intensity of the motion of the crop canopy as a function of the wind velocity: (a) dimensional data, (b) normalised data. (*) alfalfa, (o) wheat.

once again demonstrating the role of the plants' rigidity on the characteristics of their motion. The apparent shift of a few data points for wheat is likely to be caused by an underestimation of f_0 for wheat due to the biological variability of the plants' properties, as already discussed Section 2.2, and by the linearity of the model providing the instability growth rate. These experimental results can be used to validate non-linear models, which should include non-linearities in the equations for both the fluid and the solid. They can also be used by themselves as input data for thigmomorphogenesis analyses. We furthermore note that other fluid-structure interactions problems, such as the vibration of sets of elastic rods in cross flows as studied by Moon & Kuroda (2001) and, more recently, by Brücker & Smith (2005), may help understand these non-linear aspects.

Another limit of the present model is its focus on only two-dimensional primary instabilities. The mixing layer instability of wind over plant canopies rapidly becomes three-dimensional; however, the main spatio-temporal characteristics of the two-dimensional primary waves are known to be preserved in three dimensions (Finnigan 2000). The extension of the present model to include an additional degree of freedom for the plants and flow motion would constitute an interesting topic for future work. In the experiments,

we focused only on the principal streamwise wavelengths of the spatial structures but data is available to characterize the complete horizontal motion of the canopy. The full coupling between the three-dimensional instability of the wind and the two-dimensional horizontal motion of the canopy surface remains an open problem.

A plant canopy with homogeneous properties was considered in this study although crop plants are known to display a high variability of their properties. It is thus remarkable that an agreement between the results of the model and those of the experiments was reached despite the data dispersion in the sampled plants and despite the artificial homogeneity of the canopy in the theoretical model. A further extension of the model would incorporate a statistical variability of the mechanical parameters in the canopy.

5.4. Concluding remarks

The mechanical system considered in this study is quite complex in many aspects. The wind dynamics near the top of a crop canopy can be expected to behave differently from that over more classical boundaries. The canopy, modeled as a vibrating continuum made up by a large number of plants, significantly differs from structures usually considered in flow-induced vibration analyses. Each plant is mechanically unique, and the interactions between plants can be highly non-linear and dissipative. Moreover, the two mechanical components, fluid and solid, are naturally coupled through an interface of considerable complexity, consisting of the leaves and stems of all plants.

Notwithstanding this complexity, regular propagating patterns have routinely been observed on canopies, such as honamis in waving wheat. First steps toward understanding this striking simplicity were made in the pioneering work of Raupach *et al.* (1996) when measurements of wind over crops and forests showed that a mixing layer instability played a dominant role.

We have shown, both experimentally and theoretically, that the crop dynamics also

plays an important role in the build-up of these propagating patterns, through a lock-in mechanism.

The experimental approach and the model proposed here can build the foundation for the characterisation and understanding of flow-induced motion of many types of systems: natural or grown canopies under wind, submerged aquatic vegetations under sea and river currents and, more generally, dense sets of flexible systems transversely bounding a flow.

Appendix A. Dispersion relation

Below we give the terms of the dispersion relation (3.8):

$$D_{solid} = -\bar{m}\omega^2 + \bar{r},$$

$$A = -i\bar{C}\bar{h}(R-1)\omega/3,$$

$$D_{fluid} = 4k^2 (-e^{-2k}R^2 + e^{-2\bar{h}k}R((R+1)k - \omega - R) - e^{-2(1+\bar{h})k}R((1-R)k - \omega - R) + R^2 + k^2(R^2 - 1) - 2k(R^2 - \omega) - \omega^2),$$

$$E = -2i\bar{C}k^2(R-1)e^{-2(1+\bar{h})k}(1 + e^{2\bar{h}k})(R + e^{2k}((R+1)k - \omega - R))/\bar{l}^2,$$

$$G = -2\bar{C}^2\omega e^{-2(1+\bar{h})k}(e^{\bar{h}k} - 1)(R-1)^2 \left(1 + \bar{h}k + e^{\bar{h}k}(-1 + \bar{h}k)\right) (R + e^{2k}((R+1)k - \omega - R)) / \bar{h}\bar{l}^2.$$

Note that these differ slightly from Py *et al.* (2004) where one of the terms was incorrectly integrated.

Appendix B. Asymptotic analysis

The asymptotic analysis of the coupled model for a stiff canopy (section 5.2), detailed below, uses an approach introduced by Peake (1997). We assume that the stiff model (5.1) is governed by the following dispersion relation:

$$D(k, \omega) + \epsilon E(k, \omega) = 0, \tag{B1}$$

with $\epsilon \ll 1$ and where D is D_{fluid} . Let (k_0, ω_0) be the most unstable solution of D , so that

$$D(k_0, \omega_0) = 0 \quad \text{and} \quad \frac{\partial \omega_i}{\partial k}(k_0, \omega_0) = 0. \quad (\text{B } 2)$$

Including the effect of the coupling term E , the most unstable point becomes $k = k_0 + \epsilon \Delta k$, $\omega = \omega_0 + \epsilon \Delta \omega$, with $\epsilon \ll 1$, and solves the equation

$$D(k, \omega) + \epsilon E(k, \omega) = 0 \quad \text{and} \quad \frac{\partial \omega_i}{\partial k}(k, \omega) = 0. \quad (\text{B } 3)$$

The first order expansion of Eq. (B 1) near (k_0, ω_0) gives a first equation for Δk and $\Delta \omega$:

$$\Delta k D_k + \Delta \omega D_\omega + E = 0, \quad (\text{B } 4)$$

where D_j denotes the derivative of D with respect to j . Differentiating Eq. (B 1) with respect to k leads to

$$\frac{\partial \omega}{\partial k} = -\frac{D_k + \epsilon E_k}{D_\omega + \epsilon E_\omega}, \quad (\text{B } 5)$$

which, in turn, may be expanded to first order around (k_0, ω_0) (Peake 1997):

$$\frac{\partial \omega}{\partial k}(k, \omega) = -\frac{D_k}{D_\omega} + \epsilon \left(-\frac{\Delta k D_{kk} + \Delta \omega D_{k\omega} + E_k}{D_\omega} + \frac{D_k(\Delta k D_{k\omega} + \Delta \omega D_{\omega\omega} + E_\omega)}{D_\omega^2} \right). \quad (\text{B } 6)$$

Condition (B 3) requires that the imaginary part of $\partial \omega / \partial k$ is zero at (k, ω) . By definition of (k_0, ω_0) , Eq. (B 2), together with Eq. (B 4), we see that the imaginary part of $-D_k / D_\omega = \partial \omega / \partial k(k_0, \omega_0)$ is zero. We thus obtain a second equation for Δk and $\Delta \omega$:

$$\text{Im} \left[-\frac{\Delta k D_{kk} + \Delta \omega D_{k\omega} + E_k}{D_\omega} + \frac{D_k(\Delta k D_{k\omega} + \Delta \omega D_{\omega\omega} + E_\omega)}{D_\omega^2} \right] = 0. \quad (\text{B } 7)$$

Solving equations (B 4) and (B 7) finally leads to:

$$\Delta k = -\frac{\text{Im} [(ED_{k\omega}D_\omega - ED_kD_{\omega\omega} - E_kD_\omega^2 + D_kE_\omega D_\omega)/D_\omega^3]}{\text{Im} [(-D_{kk}D_\omega^2 + 2D_kD_{k\omega}D_\omega - D_k^2D_{\omega\omega})/D_\omega^3]}, \quad (\text{B } 8)$$

$$\Delta \omega = \frac{E + \Delta k D_k}{D_\omega}. \quad (\text{B } 9)$$

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